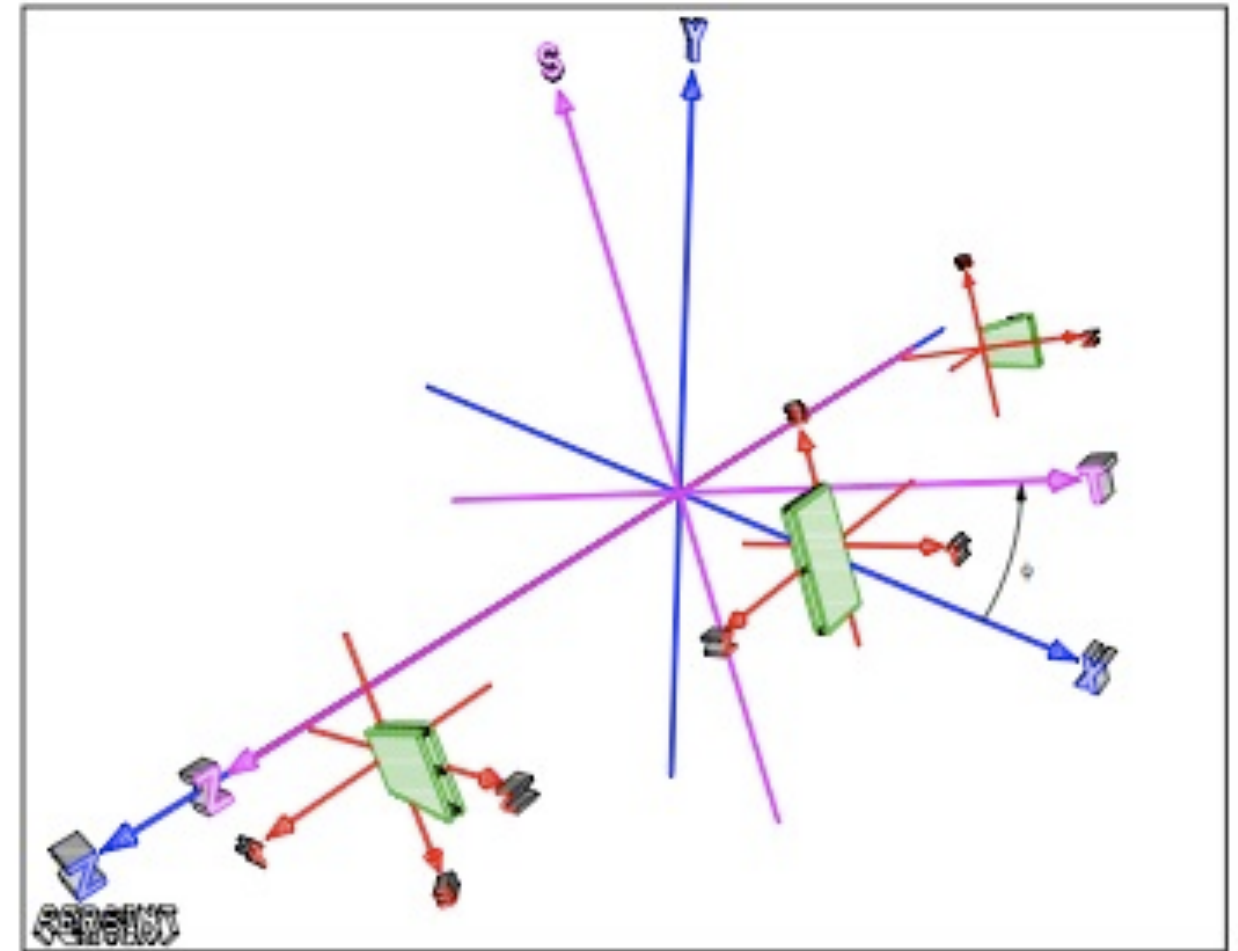


B-Lines implementation in MGM

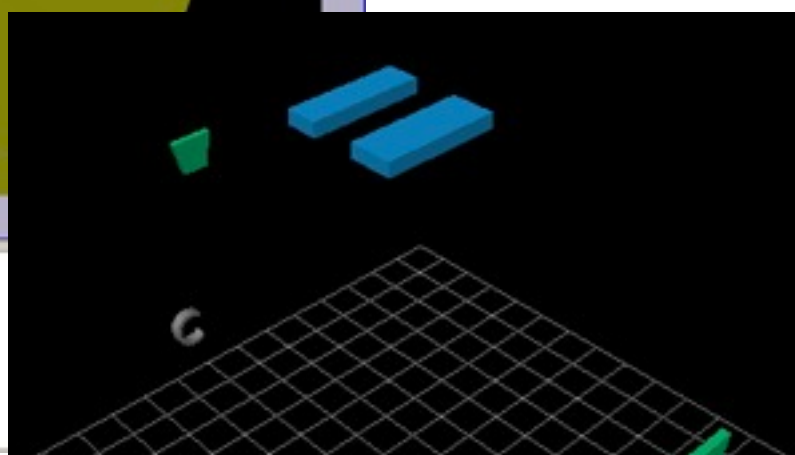
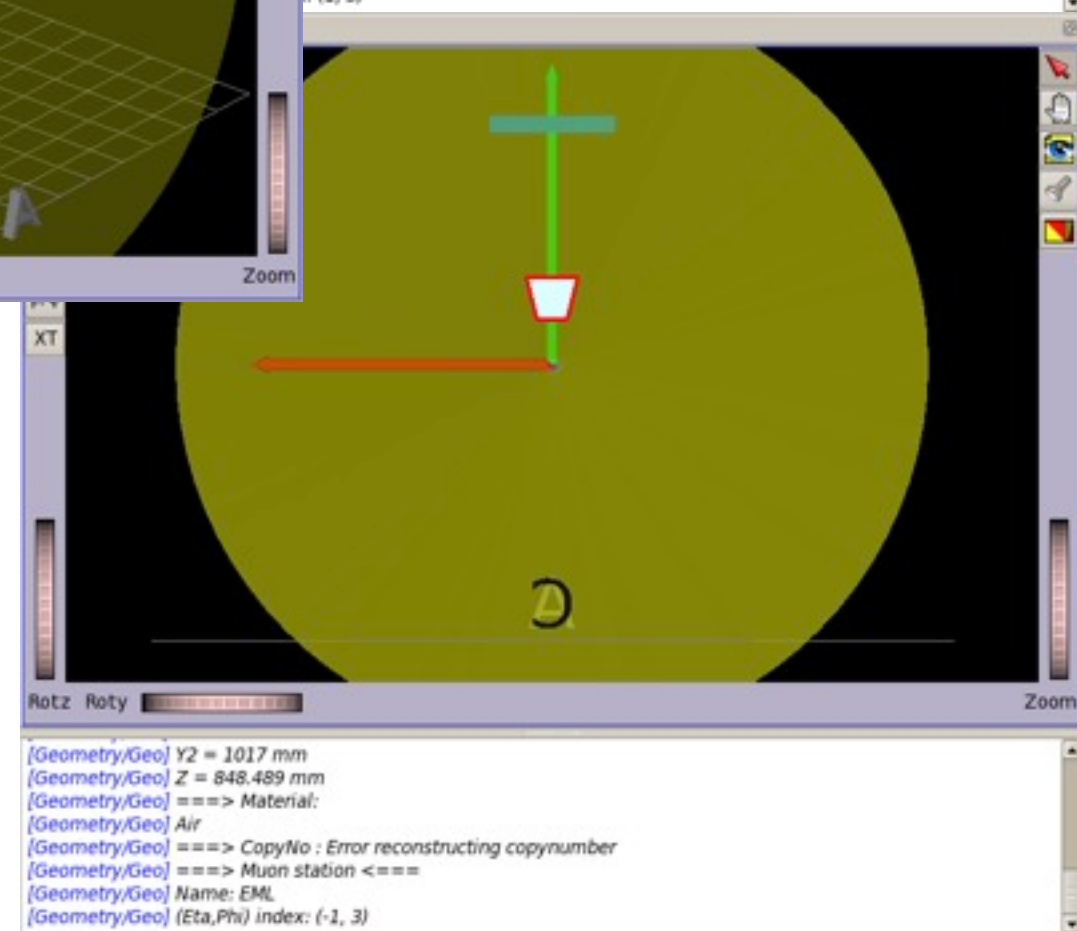
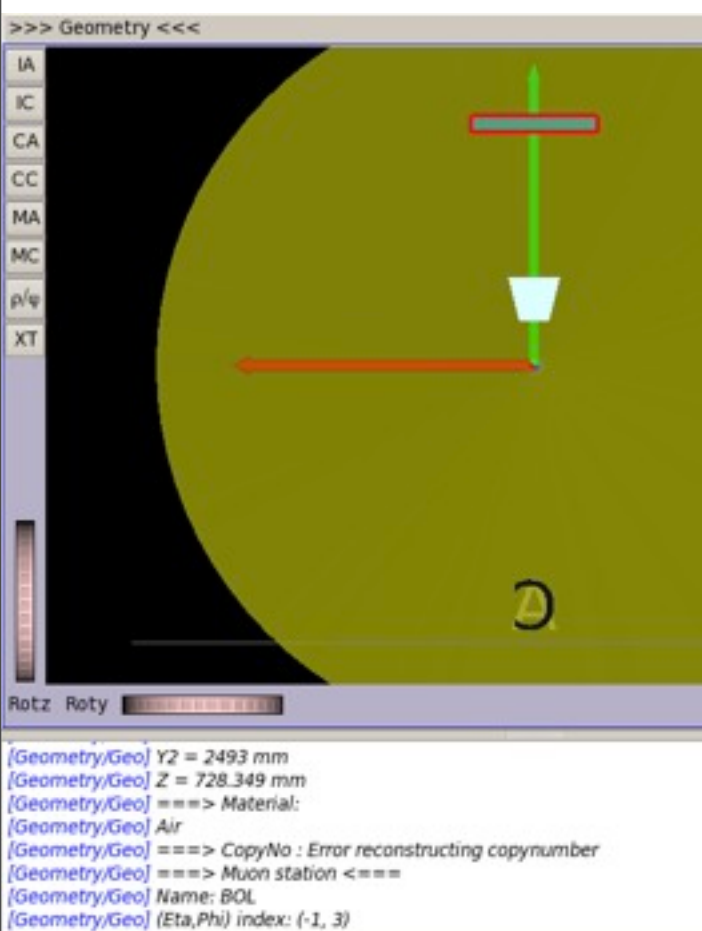
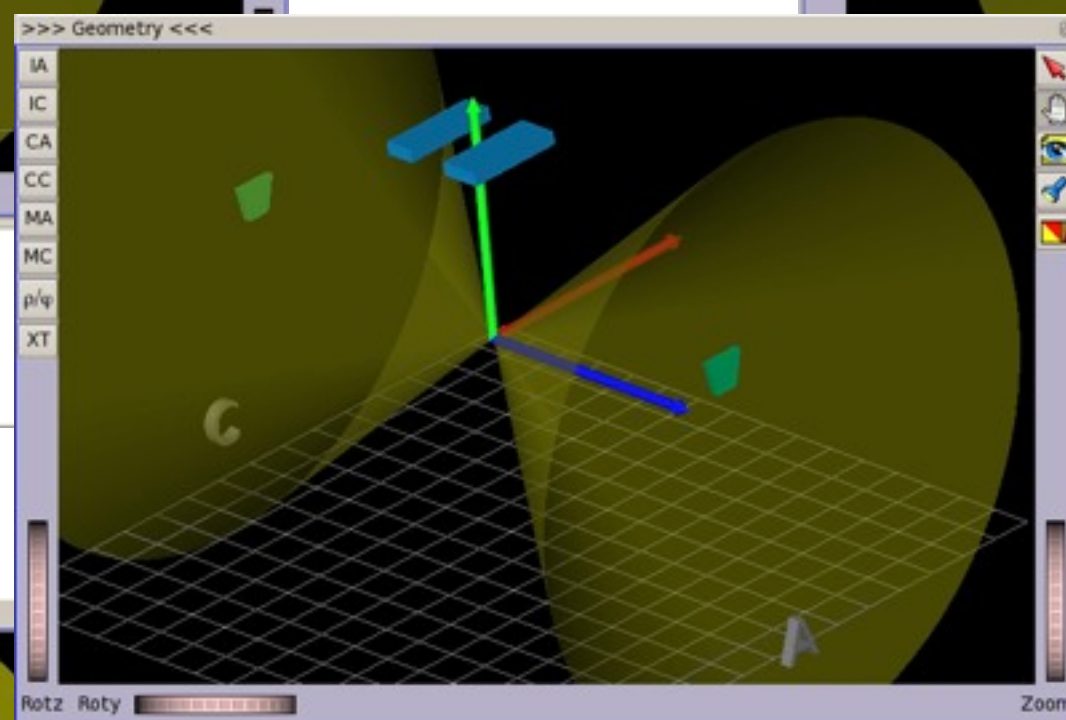
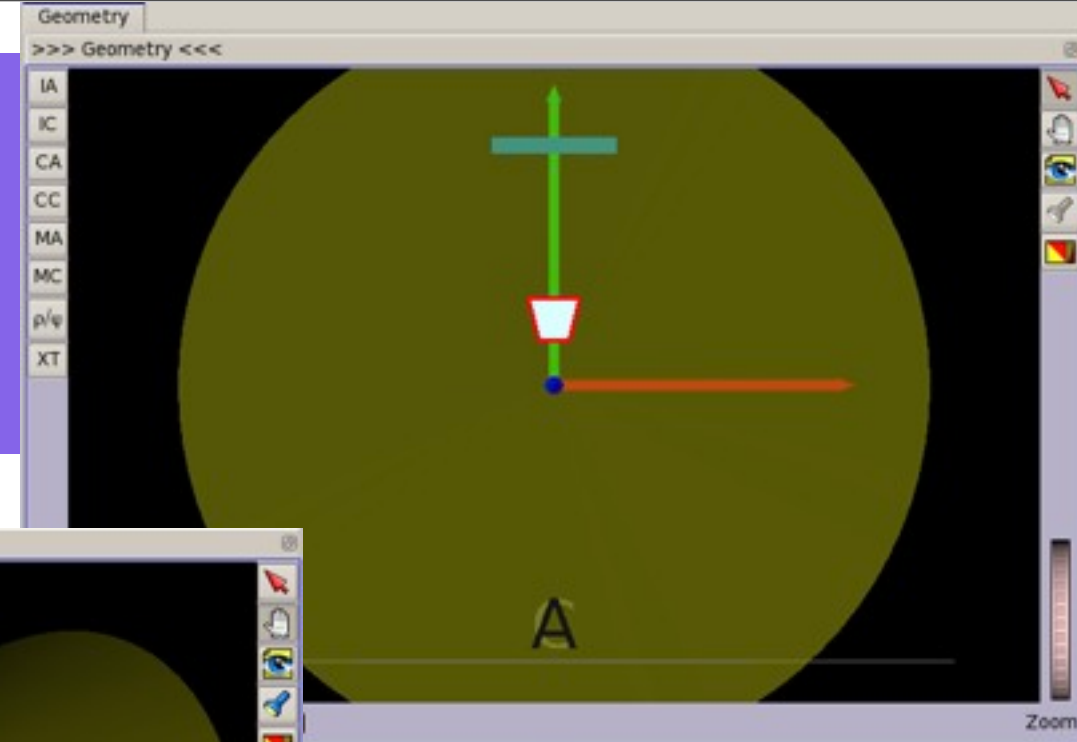
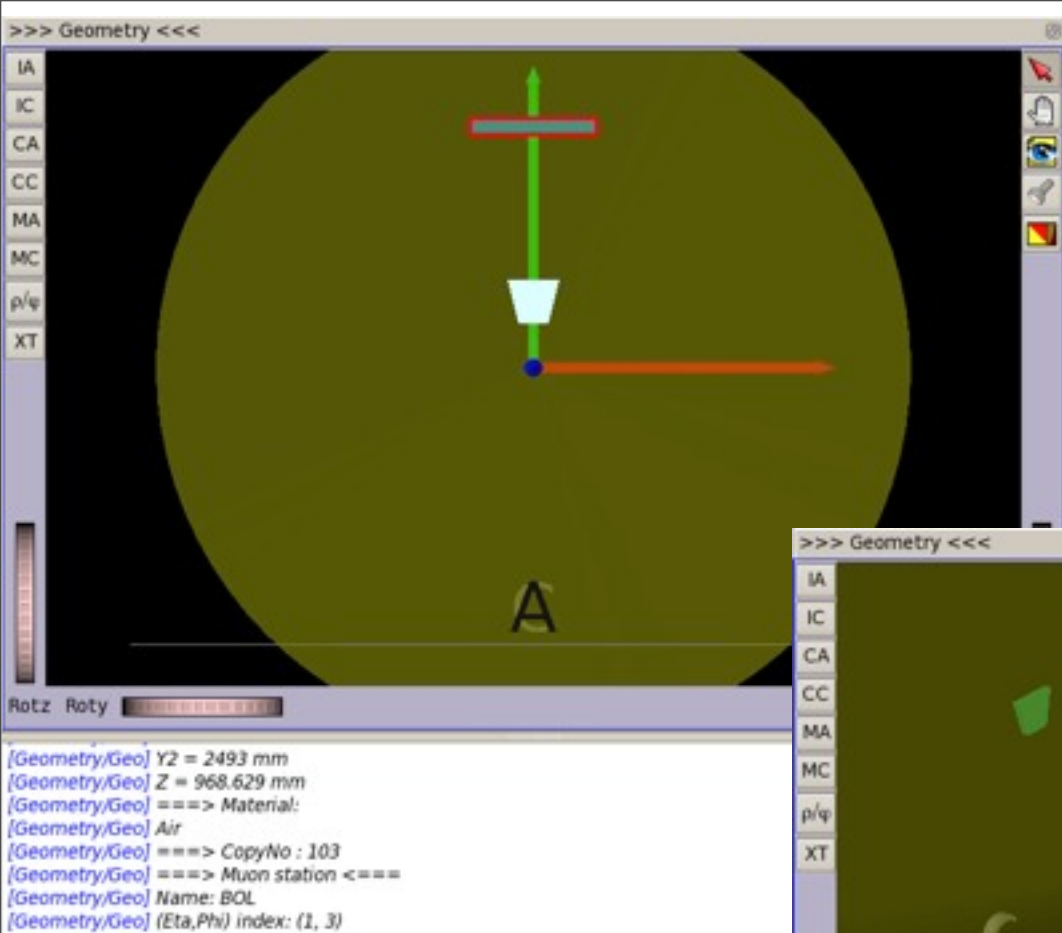
S. Spagnolo

- reminder

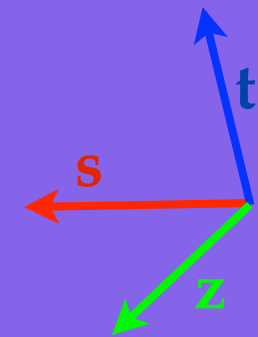


Check implementation

- Concentrate on BOL and EML in sector 5 (stationPhi=3) and StationEta=+-1 (to check both C and A side)
- Barrel, sector 5, side A \rightarrow amdb local **sz**t frame is equal (but translated) to **-x,z,y** (global ATLAS frame)
- Barrel, sector 5, side C \rightarrow amdb local **sz**t frame is equal (but translated) to **-x,z,y** (global ATLAS frame) [equal to side A]
- End-cap, sector 5, side A \rightarrow amdb local **sz**t frame is equal (but translated) to **x,y,z** (global ATLAS frame)
- End-cap, sector 5, side C \rightarrow amdb local **sz**t frame is equal (but translated) to **-x,y,-z** (global ATLAS frame)
- baseline layout: ATLAS-GEO-10-00-01, conditions



sp=10mm BOL



Cross Plate Sag out of Plane: sp,sn (2 Parameters)

• sp,sn:

sag of cross plates out of chamber plane, tubes remain straight

maximum elongation along cross plate (at center) equals sp at P-side cross-plate, and sn at N-side cross-plate, positive for sag towards negative t

unit: mm

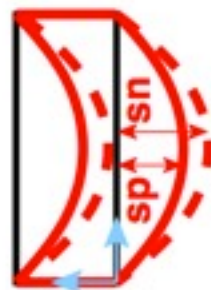
typical: $\mathcal{O}(10 \mu\text{m})$

formula:

$$\phi = \frac{1}{2}(sp + sn) \cdot (z_{\text{rel}}^2 - 1) + \frac{1}{2}(sp - sn) \cdot (z_{\text{rel}}^2 - 1) \cdot s_{\text{rel}}$$

transformation:

$$\begin{aligned} s &\rightarrow s \\ t &\rightarrow t + \phi \\ z &\rightarrow z \end{aligned}$$



sp ≠ 0 sn=0
BOL Aside

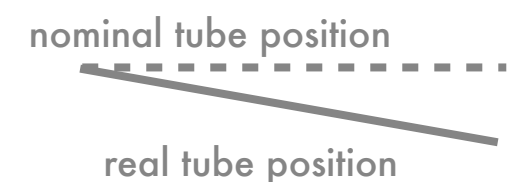
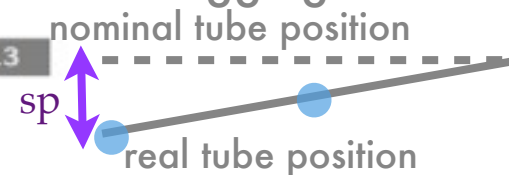
Looking from A to C side

t=y_{global}

S=-X_{global}

sp > 0 sn=0
this cross plate
is sagging

sp = 0 sn > 0
this cross plate is
sagging



FB & CA

Proposal for a Set of Deformation Parameters

slide 7 of 13

sp = 10. mm

[7.4.1.3.0.1.1.1] wire global pos (0.0000,9274.3029,405.0170) Tube length is 4961.4999

RO side tube end-point

(-2453.7500,9274.1507,405.0170)

HV side tube end-point

(2453.7500,9274.4550,405.0170)

[7.4.1.3.0.1.1.33] wire global pos (0.0000,9269.4570,1366.1370) Tube length is 4961.4999

RO side tube end-point

(-2453.7450,9264.5117,1366.1370)

HV side tube end-point

(2453.7450,9274.4023,1366.1370)

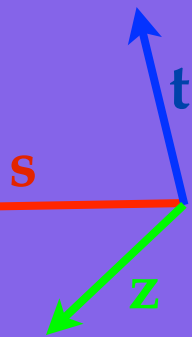
x,y,z global frame

sp = 0. mm

[7.4.1.3.0.1.1.1] wire global pos (0.0000,9274.4567,405.0170)

sp parameter implementation in barrel A and C OK

sp=10mm EML-A



Cross Plate Sag out of Plane: sp,sn (2 Parameters)

• sp,sn:

sag of cross plates out of chamber plane, tubes remain straight

maximum elongation along cross plate (at center) equals sp at P-side cross-plate, and sn at N-side cross-plate, positive for sag towards negative t

unit: mm

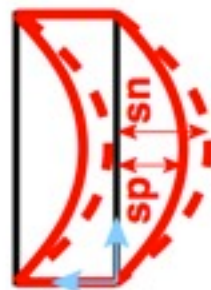
typical: $\mathcal{O}(10 \mu\text{m})$

formula:

$$\phi = \frac{1}{2}(sp + sn) \cdot (z_{\text{rel}}^2 - 1) + \frac{1}{2}(sp - sn) \cdot (z_{\text{rel}}^2 - 1) \cdot s_{\text{rel}}$$

transformation:

$$\begin{aligned} s &\rightarrow s \\ t &\rightarrow t + \phi \\ z &\rightarrow z \end{aligned}$$



sp ≠ 0 sn=0
EML Aside

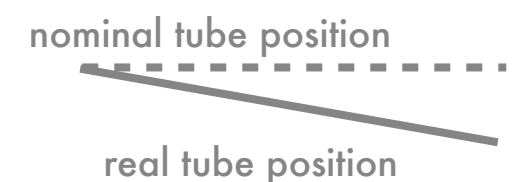
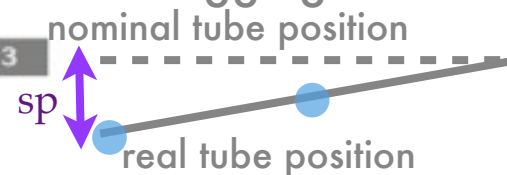
Looking radially out-in

t=z_{global}

S=X_{global}

sp > 0 sn=0
this cross plate
is sagging

sp = 0 sn > 0
this cross plate is
sagging



FB & CA

Proposal for a Set of Deformation Parameters

slide 7 of 13

sp = 10. mm

[7.17.1.3.0.1.1.1] wire global pos (0.0000,1785.0170,14142.3220) Tube length is 1186.5000

RO side tube end-point

(-566.2500,1785.0170,14142.4884)

HV side tube end-point

(566.2500,1785.0170,14142.1557)

[7.17.1.3.0.1.1.29] wire global pos (0.0000,2625.9970,14137.4979) Tube length is 1546.4999

RO side tube end-point

(-746.2356,2625.9970,14142.1210)

HV side tube end-point

(746.2356,2625.9970,14132.8747)

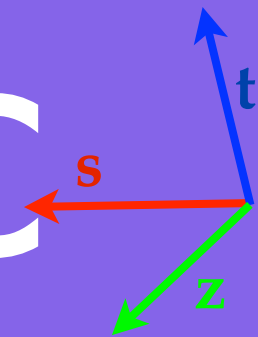
x,y,z global frame

sp = 0. mm

[7.17.1.3.0.1.1.1] wire global pos (0.0000,1785.0170,14142.3220)

sp parameter implementation in EC A OK

sp=10mm EML-C



Cross Plate Sag out of Plane: sp,sn (2 Parameters)

• sp,sn:

sag of cross plates out of chamber plane, tubes remain straight

maximum elongation along cross plate (at center) equals sp at P-side cross-plate, and sn at N-side cross-plate, positive for sag towards negative t

unit: mm

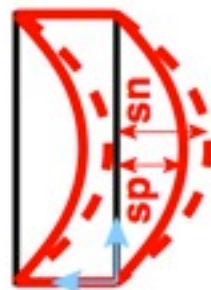
typical: $\mathcal{O}(10 \mu\text{m})$

formula:

$$\phi = \frac{1}{2}(sp + sn) \cdot (z_{\text{rel}}^2 - 1) + \frac{1}{2}(sp - sn) \cdot (z_{\text{rel}}^2 - 1) \cdot s_{\text{rel}}$$

transformation:

$$\begin{aligned} s &\rightarrow s \\ t &\rightarrow t + \phi \\ z &\rightarrow z \end{aligned}$$



sp ≠ 0 sn=0
EML Cside

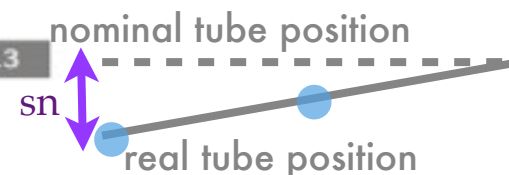
Looking radially out-in

$$t = -Z_{\text{global}}$$

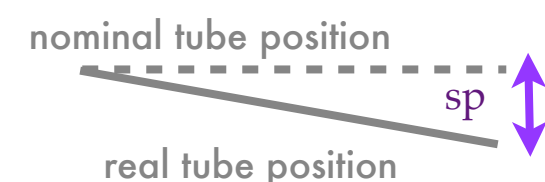
$$S = -X_{\text{global}}$$

sn > 0 sp=0
this cross plate
is sagging

sp > 0 sn = 0
this cross plate is
sagging



if tube # = Ntube/2



sp = 10. mm

[7.17.-1.3.0.1.1.1] wire global pos (0.0000,1785.0170,-14142.3220) Tube length is 1546.4999
RO side tube end-point (-566.2500,1785.0170,-14142.1557)
HV side tube end-point (566.2500,1785.0170,-14142.4884)
[7.17.-1.3.0.1.1.29] wire global pos (0.0000,2625.9970,-14137.4979) Tube length is 1546.4999
RO side tube end-point (-746.2356,2625.9970,-14132.8747)
HV side tube end-point (746.2356,2625.9970,-14142.1210)

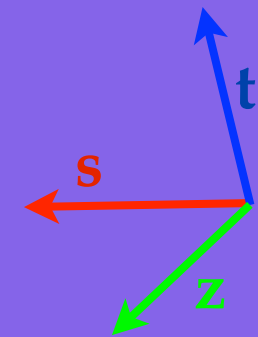
x,y,z global frame

sp = 0. mm

[7.17.-1.3.0.1.1.1] wire global pos (0.0000,1785.0170,-14142.3220)

sp parameter implementation in EC C OK

sn=20mm BOL



Cross Plate Sag out of Plane: sp,sn (2 Parameters)

• sp,sn:

sag of cross plates out of chamber plane, tubes remain straight

maximum elongation along cross plate (at center) equals sp at P-side cross-plate, and sn at N-side cross-plate, positive for sag towards negative t

unit: mm

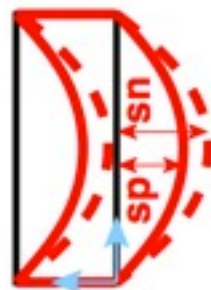
typical: $\mathcal{O}(10 \mu\text{m})$

formula:

$$\phi = \frac{1}{2}(sp + sn) \cdot (z_{\text{rel}}^2 - 1) + \frac{1}{2}(sp - sn) \cdot (z_{\text{rel}}^2 - 1) \cdot s_{\text{rel}}$$

transformation:

$$\begin{aligned} s &\rightarrow s \\ t &\rightarrow t + \phi \\ z &\rightarrow z \end{aligned}$$



sp=0 sn>0
BOL Aside

Looking from A to C side

t=y_{global}

S=-X_{global}

sp > 0 sn=0
this cross plate
is sagging

sp = 0 sn > 0
this cross plate is
sagging

nominal tube position

real tube position

if tube # = N_{tube}/2

nominal tube position

real tube position

sn = 20. mm

[7.4.1.3.0.1.1.1] wire global pos (0.0000,9274.1490,405.0170) Tube length is 4961.4999

RO side tube end-point (-2453.7500,9274.4533,405.0170)

HV side tube end-point (2453.7500,9273.8447,405.0170)

[7.4.1.3.0.1.1.33] wire global pos (0.0000,9264.4573,1366.1370) Tube length is 4961.4999

RO side tube end-point (-2453.7300,9274.3478,1366.1370)

HV side tube end-point (2453.7300,9254.5668,1366.1370)

7.4.-1.3.0.1.1.33] wire global pos (0.0000,9265.7586,-2566.1368) Tube length is 4961.4999

RO side tube end-point (-2453.7349,9274.3620,-2566.1368)

HV side tube end-point (2453.7349,9257.1553,-2566.1368)

[7.4.1.3.0.1.1.1] wire global pos (0.0000,9274.4567,405.0170)

sn = 0. mm

sn parameter implementation in barrel A and C OK

sn=10mm EML-A



Cross Plate Sag out of Plane: sp,sn (2 Parameters)

• sp,sn:

sag of cross plates out of chamber plane, tubes remain straight

maximum elongation along cross plate (at center) equals sp at P-side cross-plate, and sn at N-side cross-plate, positive for sag towards negative t

unit: mm

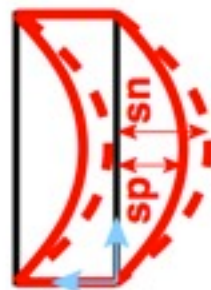
typical: $\mathcal{O}(10 \mu\text{m})$

formula:

$$\phi = \frac{1}{2}(sp + sn) \cdot (z_{\text{rel}}^2 - 1) + \frac{1}{2}(sp - sn) \cdot (z_{\text{rel}}^2 - 1) \cdot s_{\text{rel}}$$

transformation:

$$\begin{aligned} s &\rightarrow s \\ t &\rightarrow t + \phi \\ z &\rightarrow z \end{aligned}$$



sp ≠ 0 sn=0
EML Aside

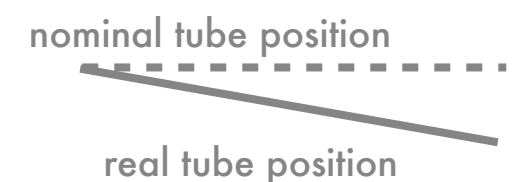
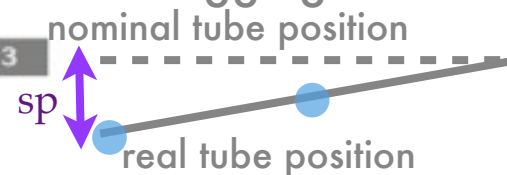
Looking radially out-in

t=Z_{global}

S=X_{global}

sp > 0 sn=0
this cross plate
is sagging

sp = 0 sn > 0
this cross plate is
sagging



FB & CA

Proposal for a Set of Deformation Parameters

slide 7 of 13

sp = 10. mm

[7.17.1.3.0.1.1.1] wire global pos (0.0000,1785.0170,14142.3220) Tube length is 1186.5000

RO side tube end-point

(-566.2500,1785.0170,14142.4884)

HV side tube end-point

(566.2500,1785.0170,14142.1557)

[7.17.1.3.0.1.1.29] wire global pos (0.0000,2625.9970,14137.4979) Tube length is 1546.4999

RO side tube end-point

(-746.2356,2625.9970,14142.1210)

HV side tube end-point

(746.2356,2625.9970,14132.8747)

x,y,z global frame

sp = 0. mm

[7.17.1.3.0.1.1.1] wire global pos (0.0000,1785.0170,14142.3220)

sp parameter implementation in EC A OK

All numbers from MGM

http://www.fisica.unisalento.it/~spagnolo/allow_listing/MDTDeformations/

Files named mdt_current_EP_*
contain

[atlas id of the tube] xRO, yRO, zRO, xCenter, yCenter, zCenter, xHV, yHV, zHV
for all tubes of

BOL in sector 5 at eta + and -1, i.e. [7.4.eta.3.0.1.1.tube#]












EML in sector 5 at eta + and -1, i.e. [7.17.eta.3.0.1.1.tube#]

coordinates are in the global ATLAS reference frame

Each file corresponds to a single B-line parameter being different than 0, value in the file name

Files named mdt_current_R.03_13_*

contains similar info with a few more details including A and B lines used

	mdt_current_EP_R.03.13_NO_blines
	mdt_current_EP_R.03.13_pg10
	mdt_current_EP_R.03.13_sn20
	mdt_current_EP_R.03.13_sp10
	mdt_current_EP_R.03.13_tr20
	mdt_current_EP_R.03.13_tw30
	mdt_current_R.03.13_pg10
	mdt_current_R.03.13_sn20
	mdt_current_R.03.13_sp10
	mdt_current_R.03.13_tr20
	mdt_current_R.03.13_tw30

Numbers from MGM **example**

mdt_current_EP_R.03.13_NO_blines **reference**

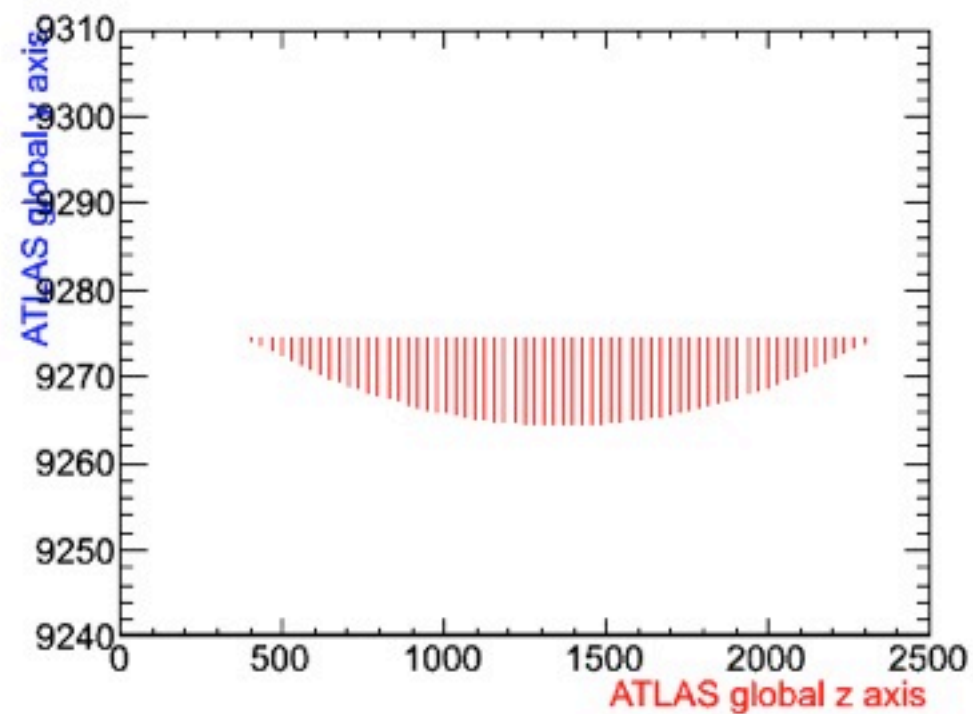
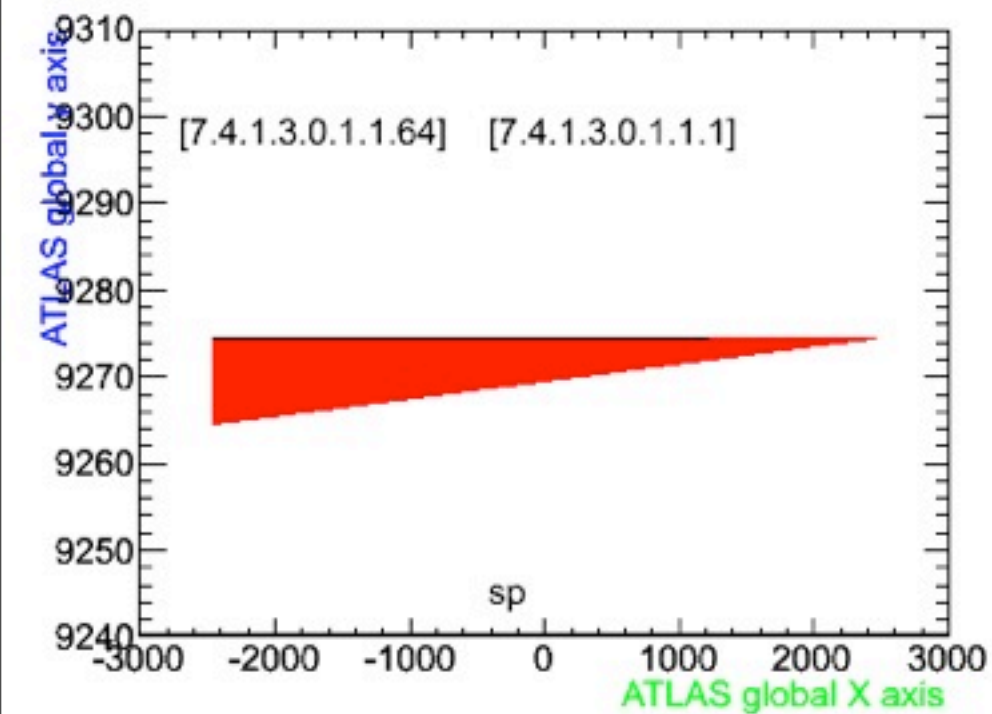
[7.4.-1.3.0.1.1.1]	-2453.7500	9274.4567	-1605.0168	0.0000	9274.4567	-1605.0168	2453.7500	9274.4567	-1605.0168
[7.4.-1.3.0.1.1.2]	-2453.7500	9274.4567	-1635.0518	0.0000	9274.4567	-1635.0518	2453.7500	9274.4567	-1635.0518
[7.4.-1.3.0.1.1.3]	-2453.7500	9274.4567	-1665.0868	0.0000	9274.4567	-1665.0868	2453.7500	9274.4567	-1665.0868
[7.4.-1.3.0.1.1.4]	-2453.7500	9274.4567	-1695.1218	0.0000	9274.4567	-1695.1218	2453.7500	9274.4567	-1695.1218
[7.4.-1.3.0.1.1.5]	-2453.7500	9274.4567	-1725.1568	0.0000	9274.4567	-1725.1568	2453.7500	9274.4567	-1725.1568
[7.4.-1.3.0.1.1.6]	-2453.7500	9274.4567	-1755.1918	0.0000	9274.4567	-1755.1918	2453.7500	9274.4567	-1755.1918
[7.4.-1.3.0.1.1.7]	-2453.7500	9274.4567	-1785.2268	0.0000	9274.4567	-1785.2268	2453.7500	9274.4567	-1785.2268
[7.4.-1.3.0.1.1.8]	-2453.7500	9274.4567	-1815.2618	0.0000	9274.4567	-1815.2618	2453.7500	9274.4567	-1815.2618
[7.4.-1.3.0.1.1.9]	-2453.7500	9274.4567	-1845.2968	0.0000	9274.4567	-1845.2968	2453.7500	9274.4567	-1845.2968

distance of RO or HV side from tube center in ideal geometry

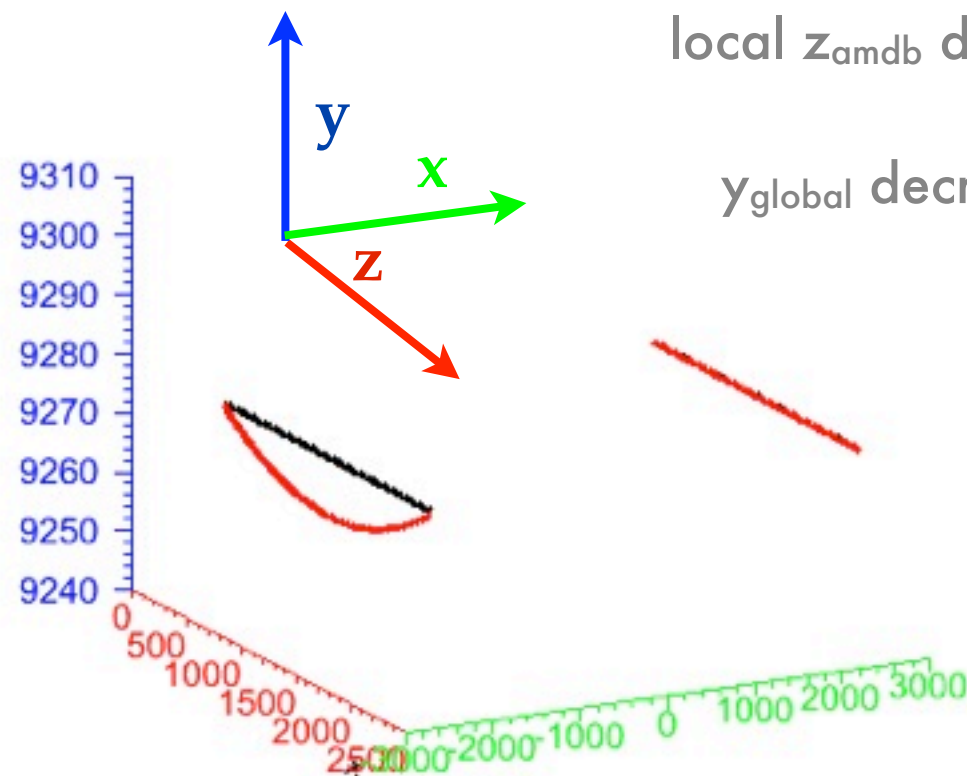
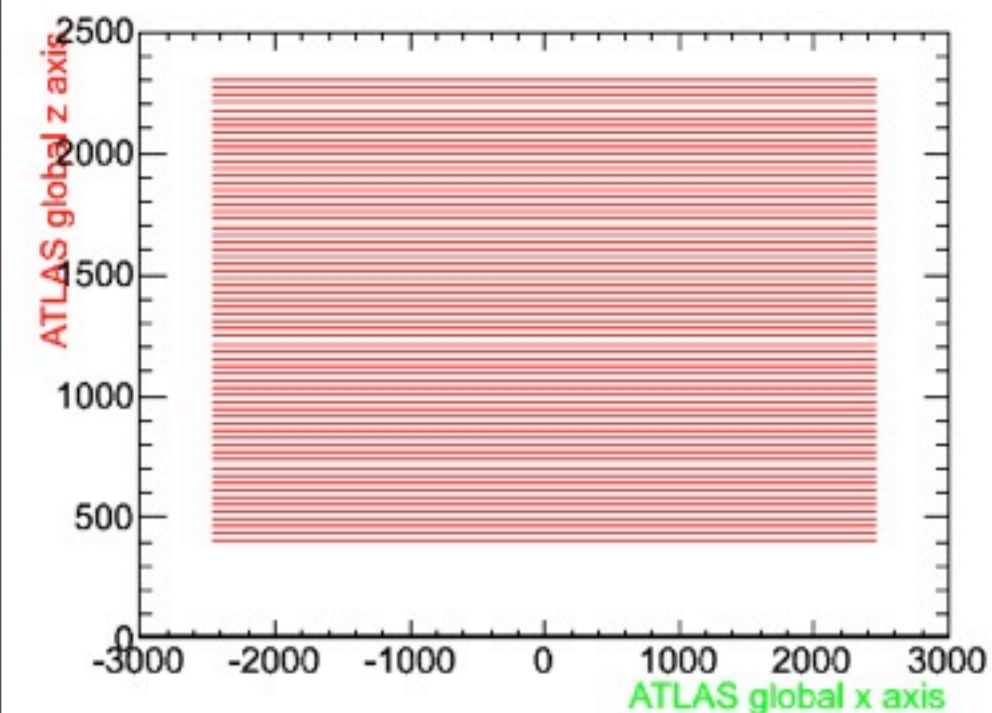
mdt_current_EP_R.03.13_tw30

[7.4.-1.3.0.1.1.1]	-2453.5849	9246.0088	-1605.7710	0.0000	9274.4567	-1605.0168	2453.5849	9302.9046	-1604.2627
[7.4.-1.3.0.1.1.2]	-2453.5988	9247.2322	-1635.8060	0.0000	9274.4567	-1635.0518	2453.5988	9301.6812	-1634.2977
[7.4.-1.3.0.1.1.3]	-2453.6121	9248.4556	-1665.8410	0.0000	9274.4567	-1665.0868	2453.6121	9300.4578	-1664.3327
[7.4.-1.3.0.1.1.4]	-2453.6247	9249.6790	-1695.8760	0.0000	9274.4567	-1695.1218	2453.6247	9299.2343	-1694.3677
[7.4.-1.3.0.1.1.5]	-2453.6368	9250.9025	-1725.9110	0.0000	9274.4567	-1725.1568	2453.6368	9298.0109	-1724.4027
[7.4.-1.3.0.1.1.6]	-2453.6482	9252.1260	-1755.9460	0.0000	9274.4567	-1755.1918	2453.6482	9296.7874	-1754.4377

sp=10mm BOLA

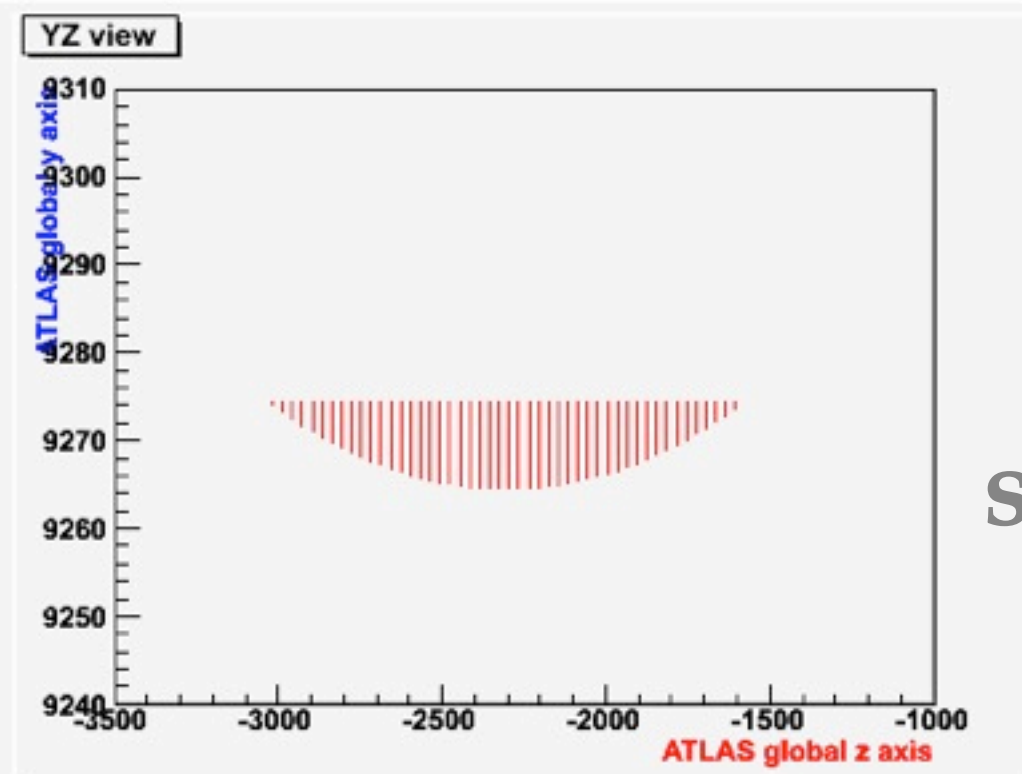
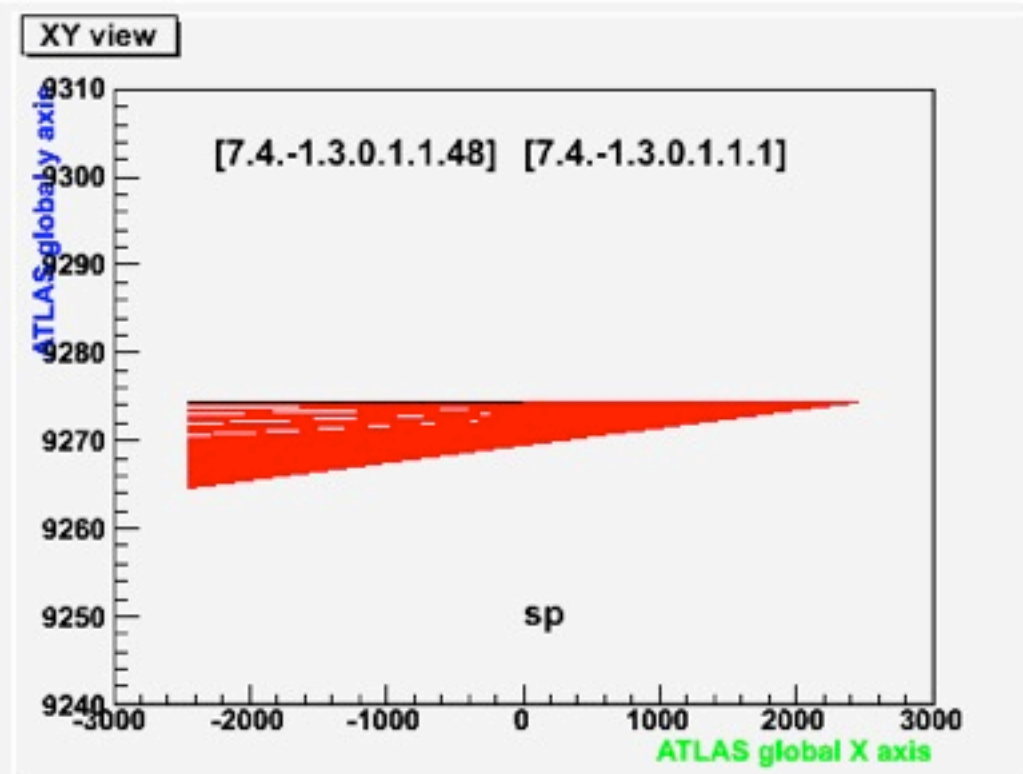


szl $\rightarrow -x, z, y$

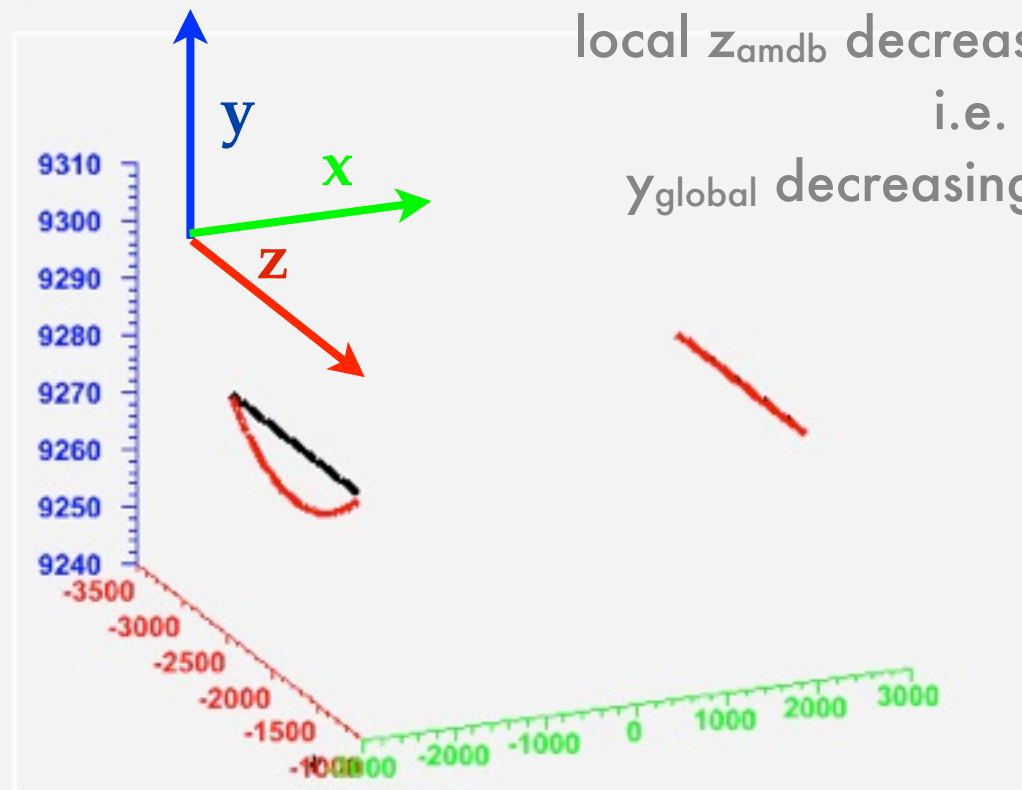
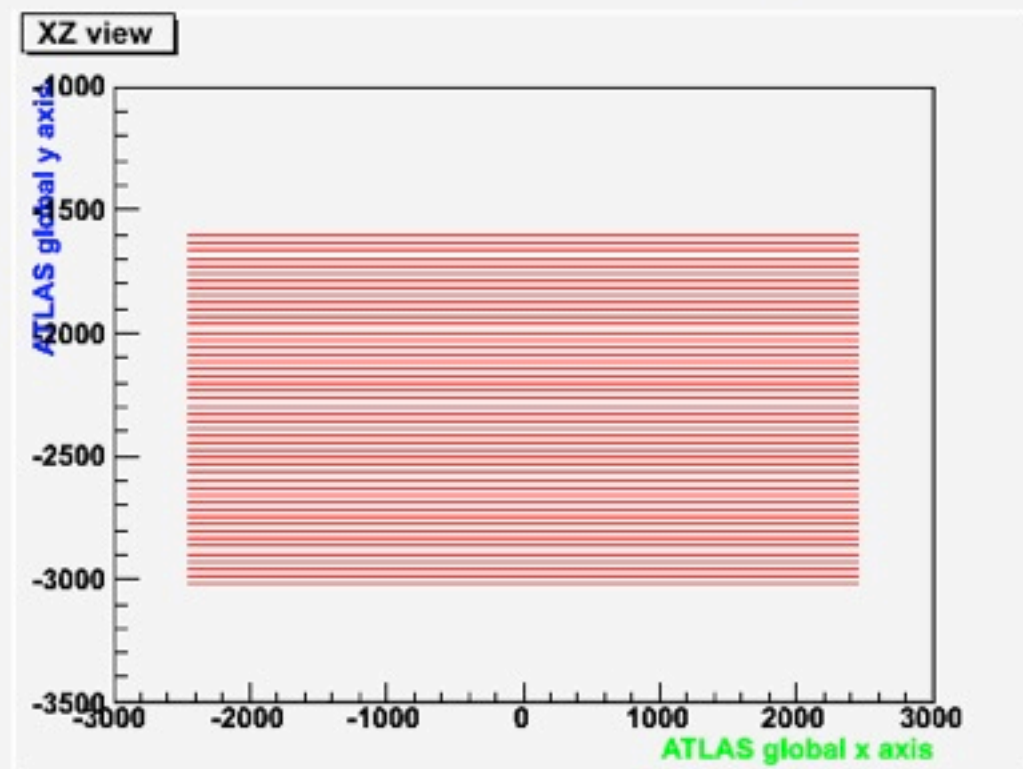


local z_{amdb} decreasing at $s_{amdb} > 0$
i.e.
 y_{global} decreasing at $x_{global} < 0$

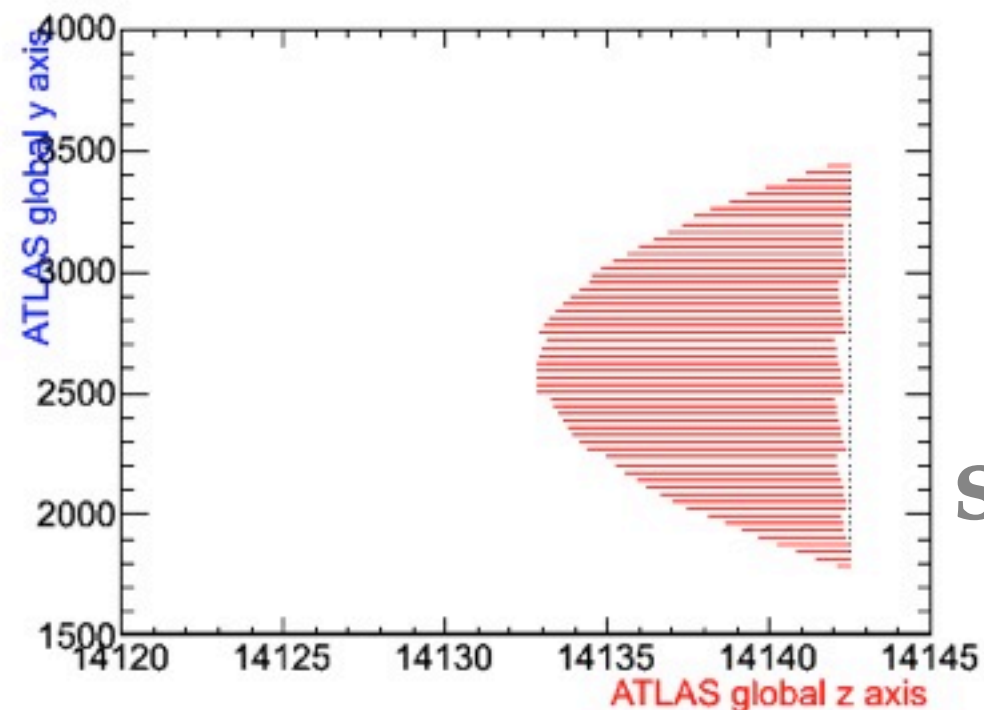
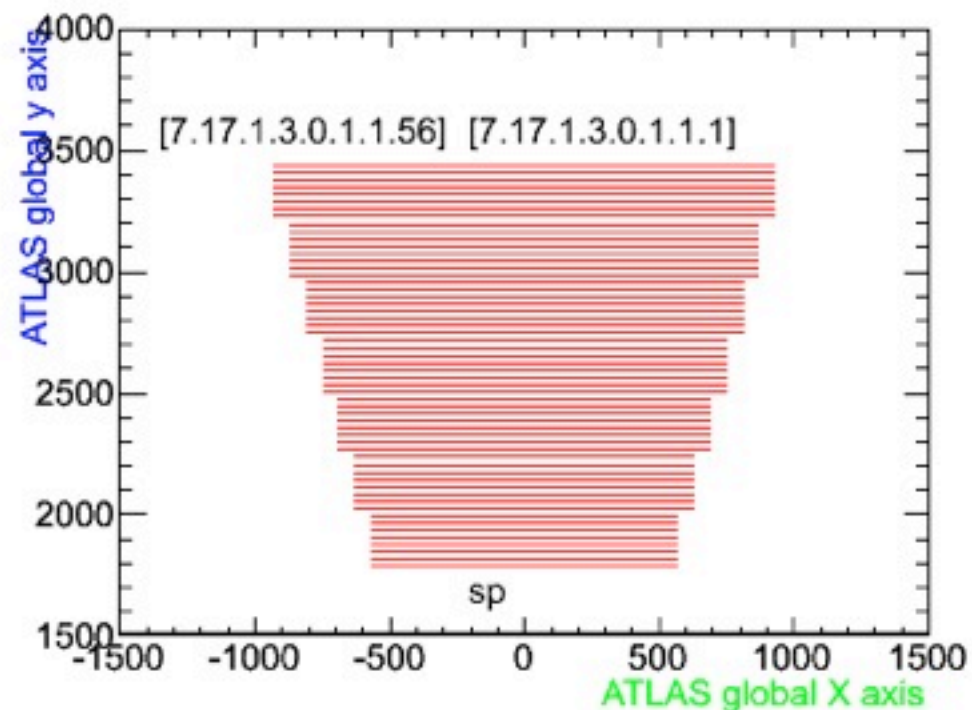
sp=10mm BOLC



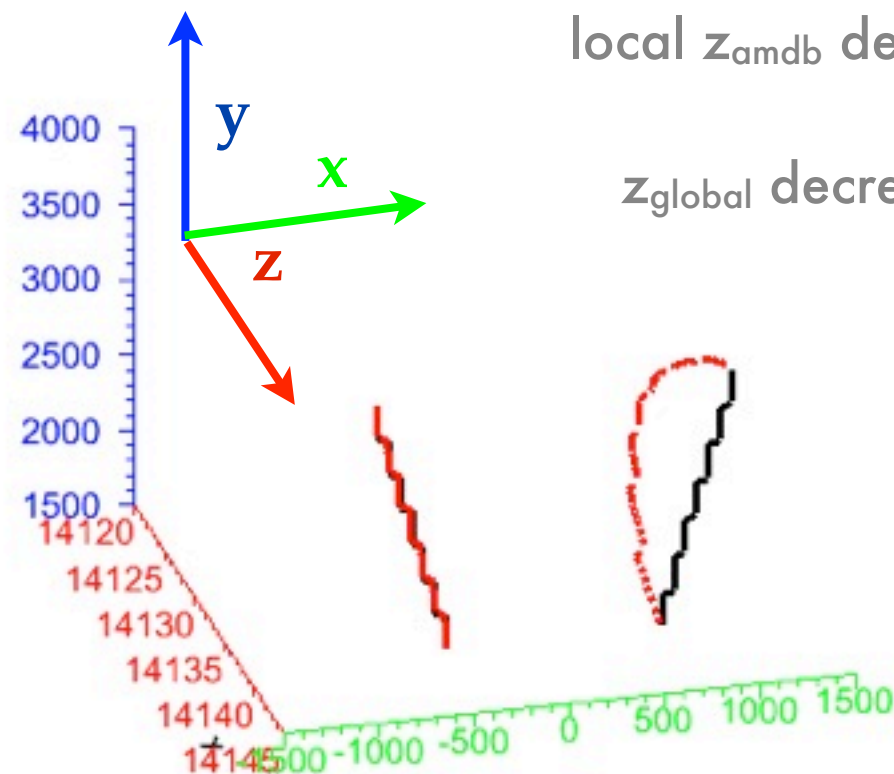
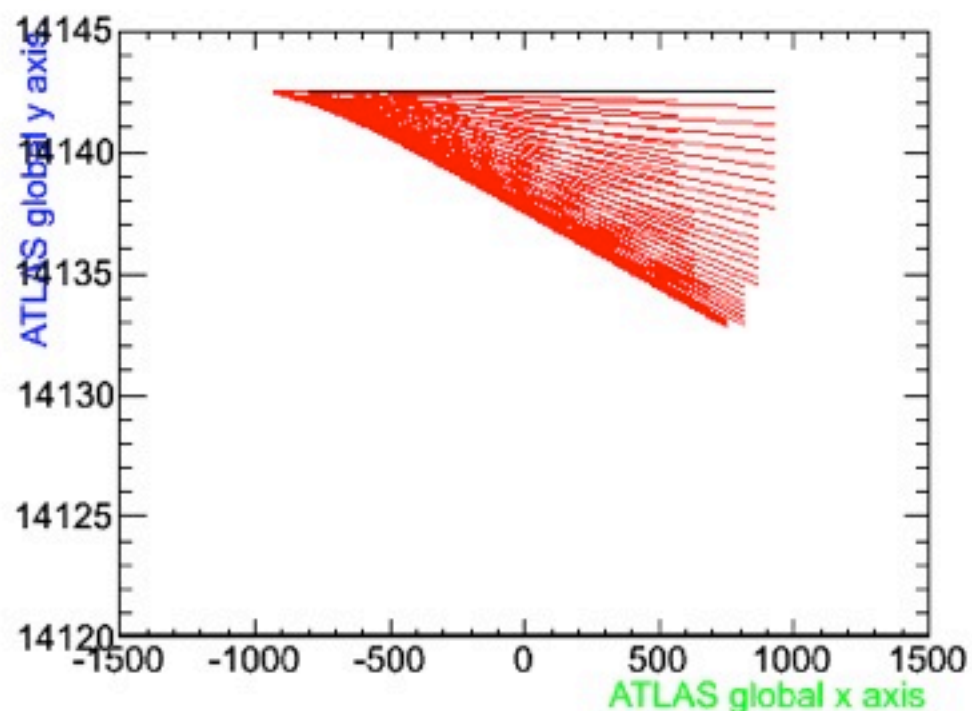
sz t $\rightarrow -x, z, y$



sp=10mm EMLA

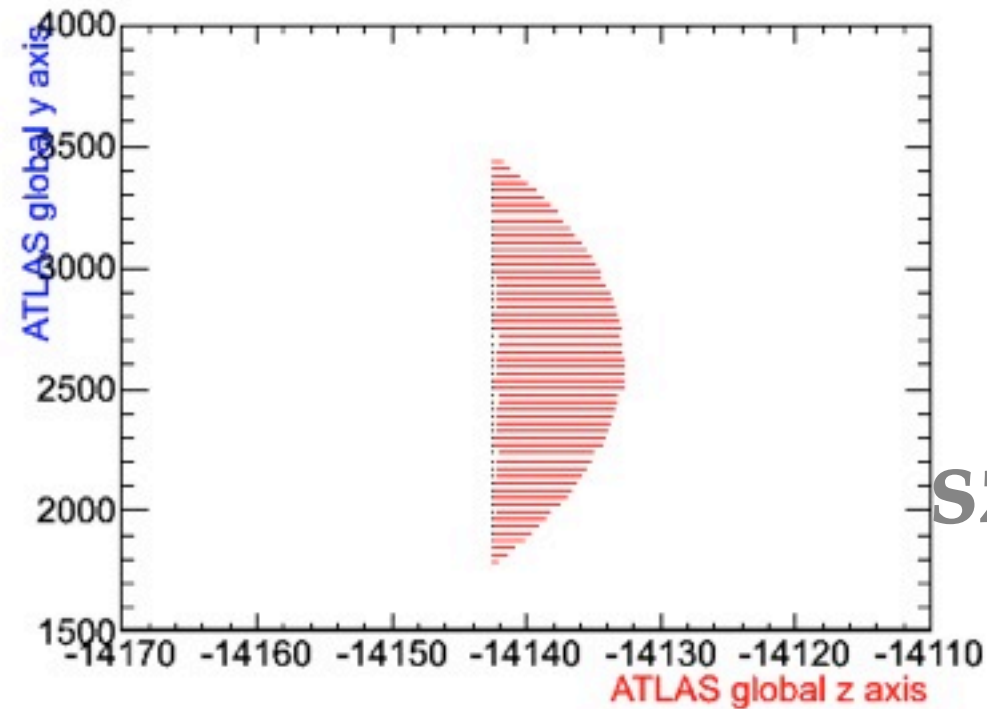
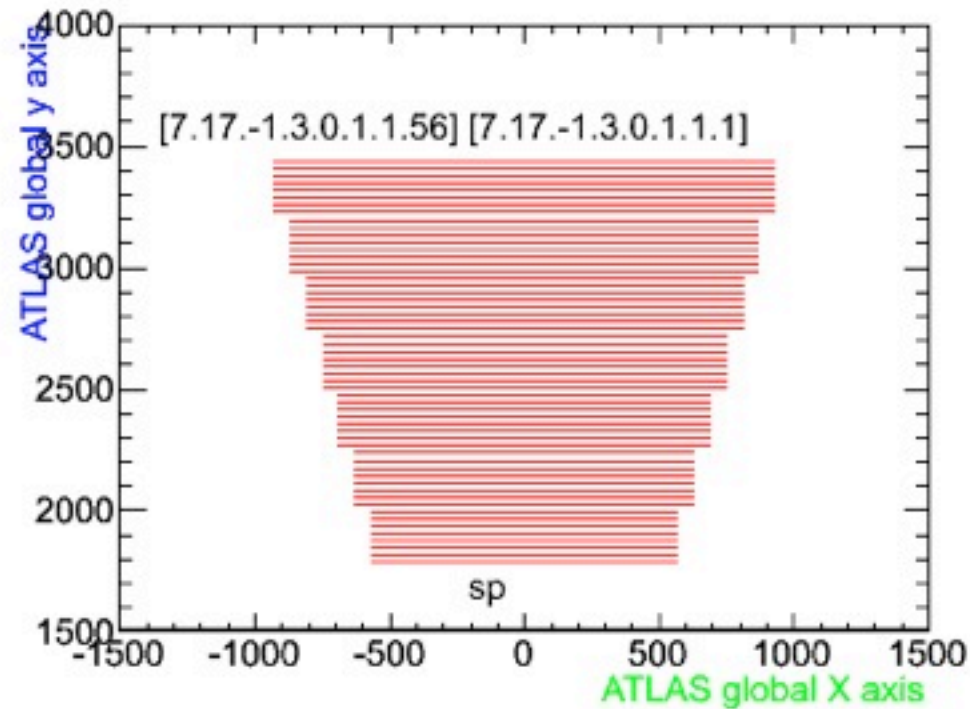


szl $\rightarrow x, z, y$

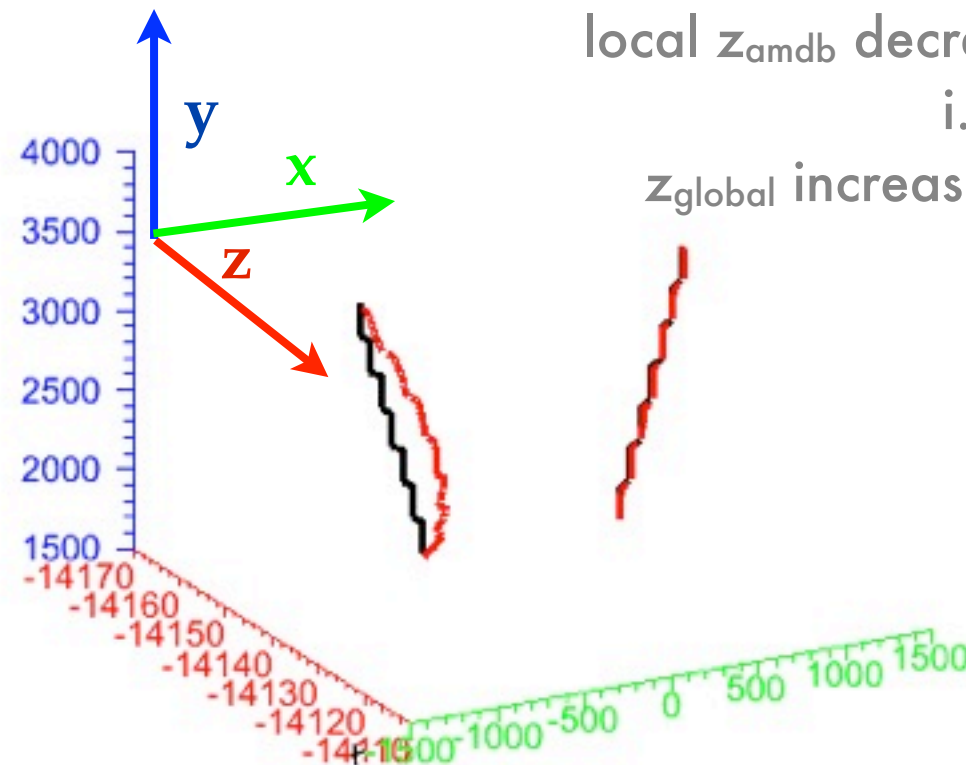
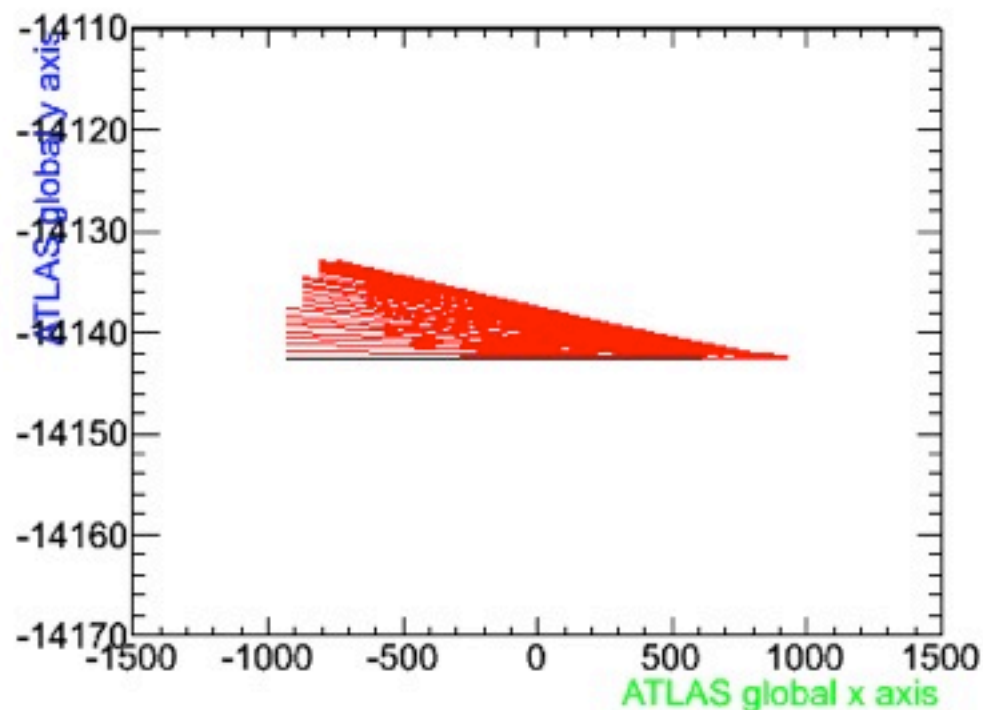


local z_{amdb} decreasing at $s_{amdb} > 0$
i.e.
 z_{global} decreasing at $x_{global} > 0$

sp=10mm EMLC



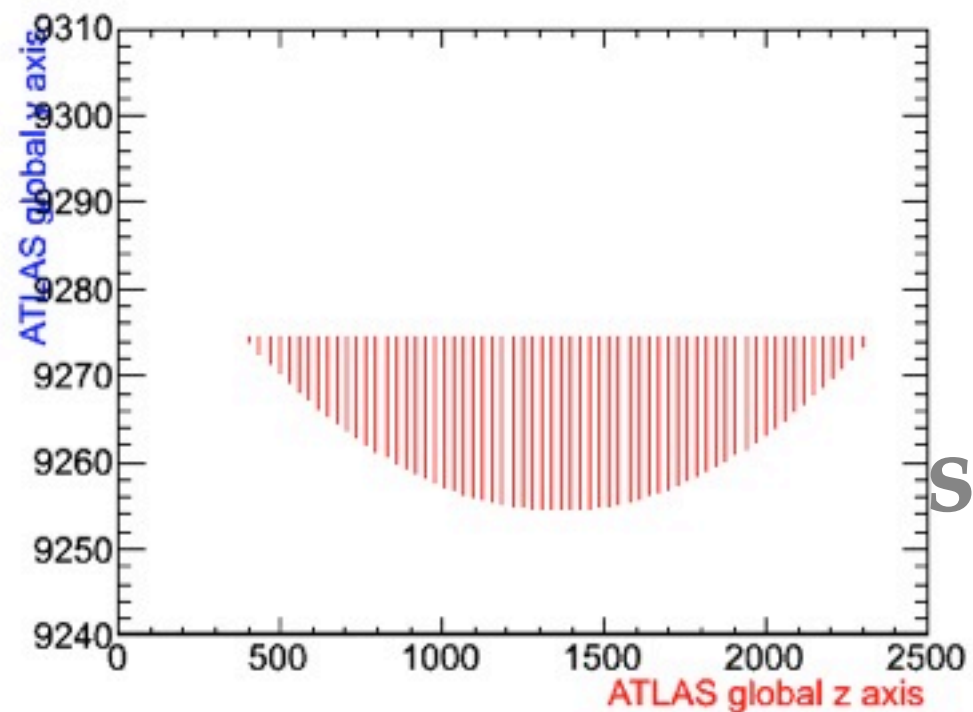
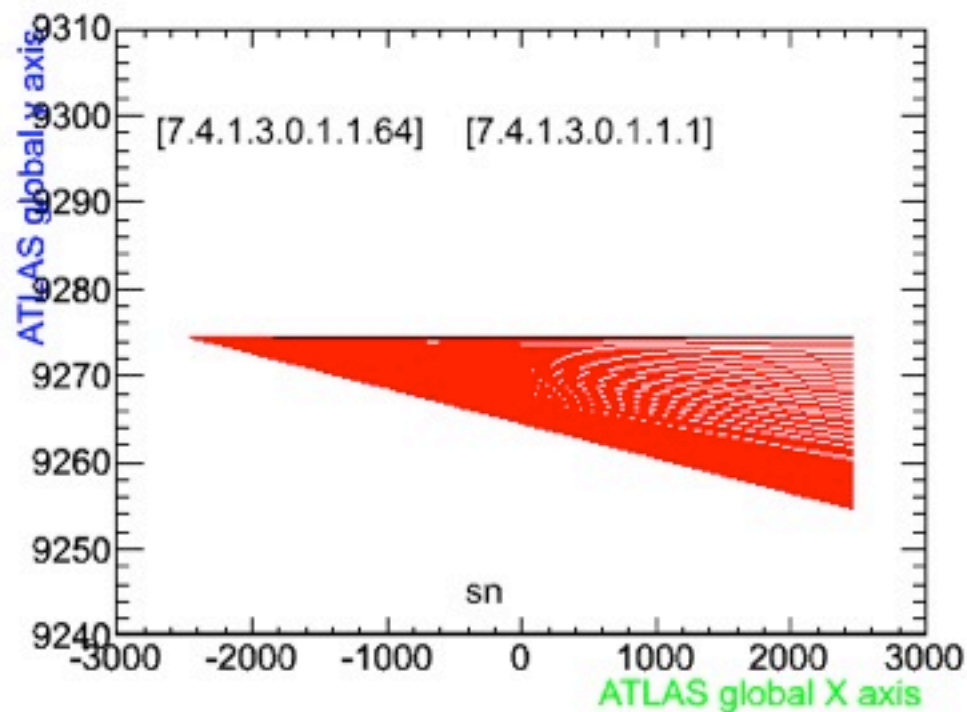
szl $\rightarrow -x, z, -y$



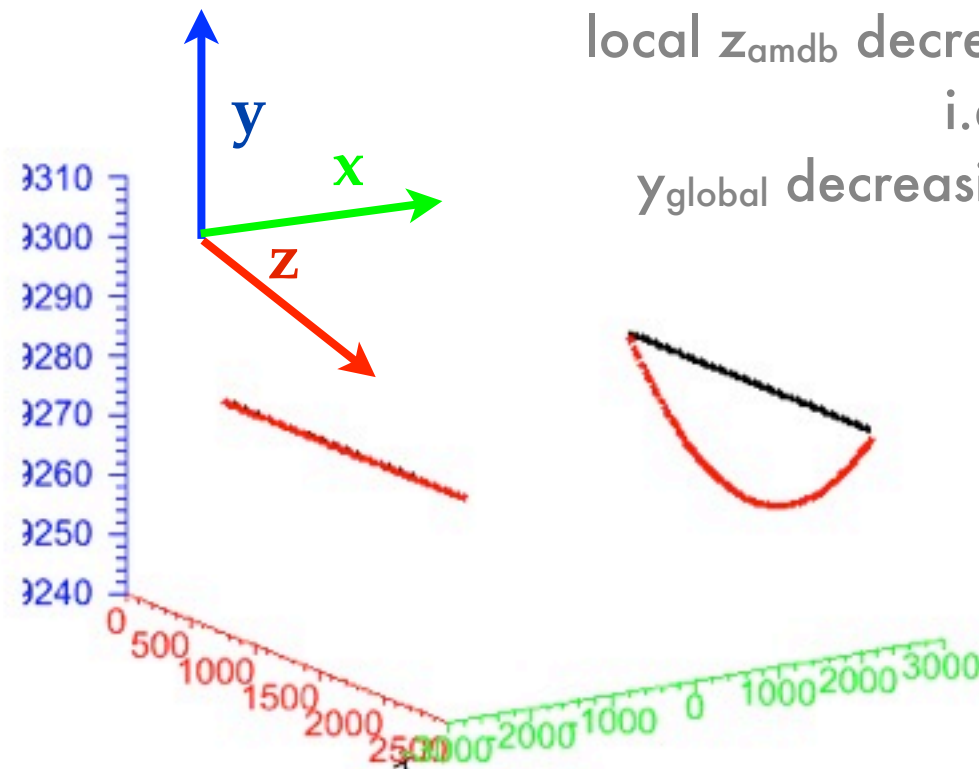
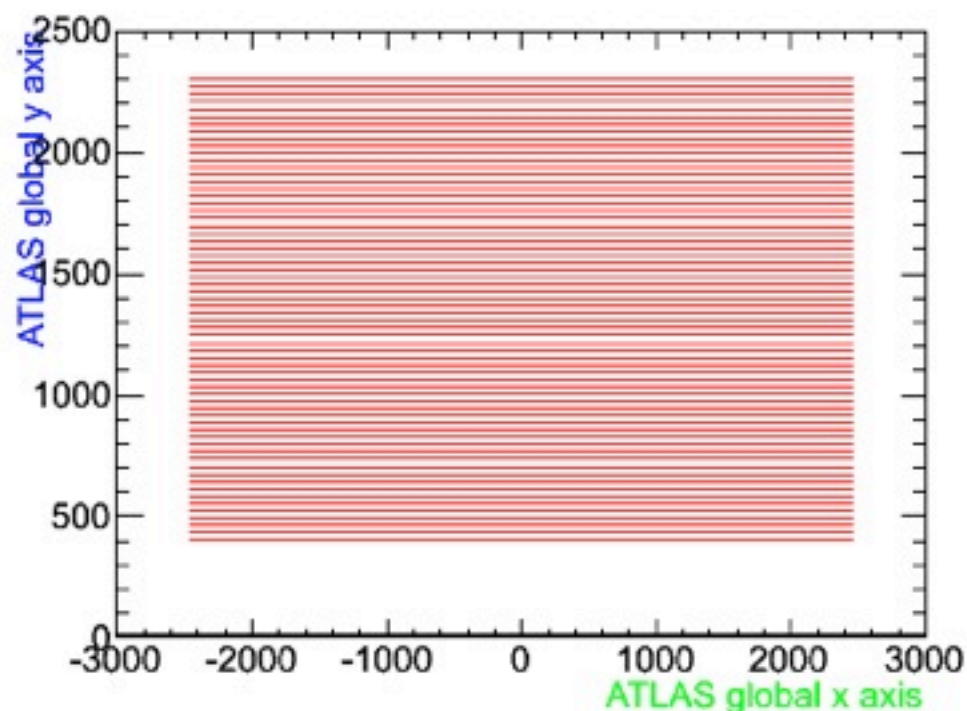
local z_{amdb} decreasing at $s_{amdb} > 0$
i.e.

z_{global} increasing at $x_{global} < 0$

sn=10mm BOLA

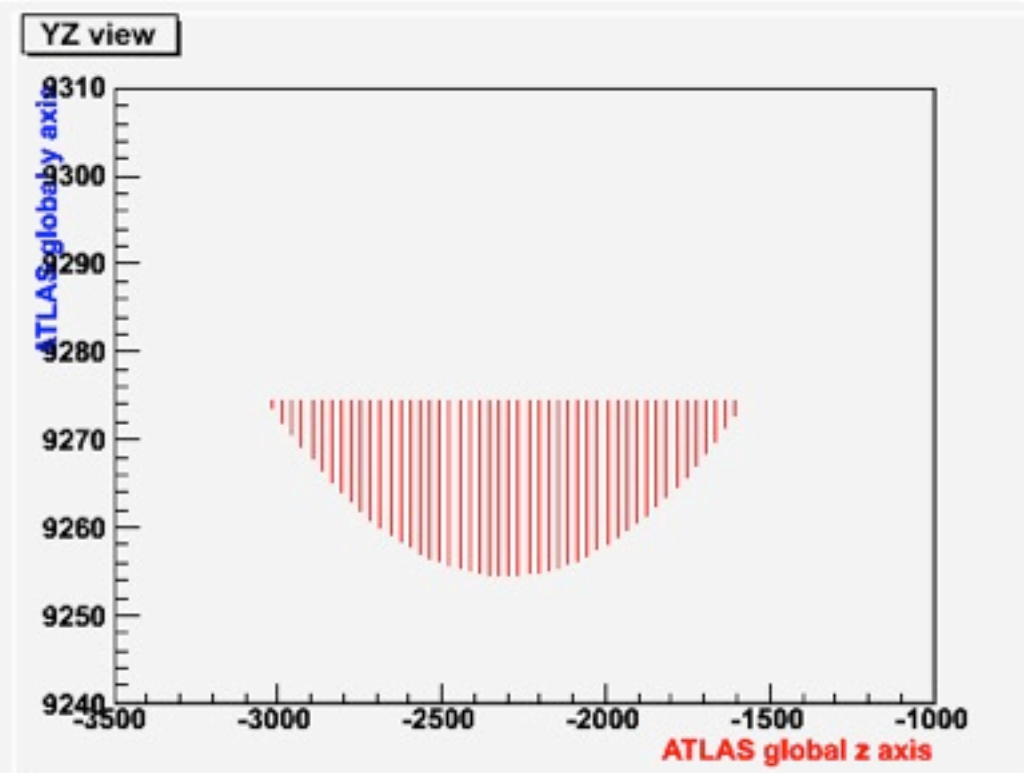
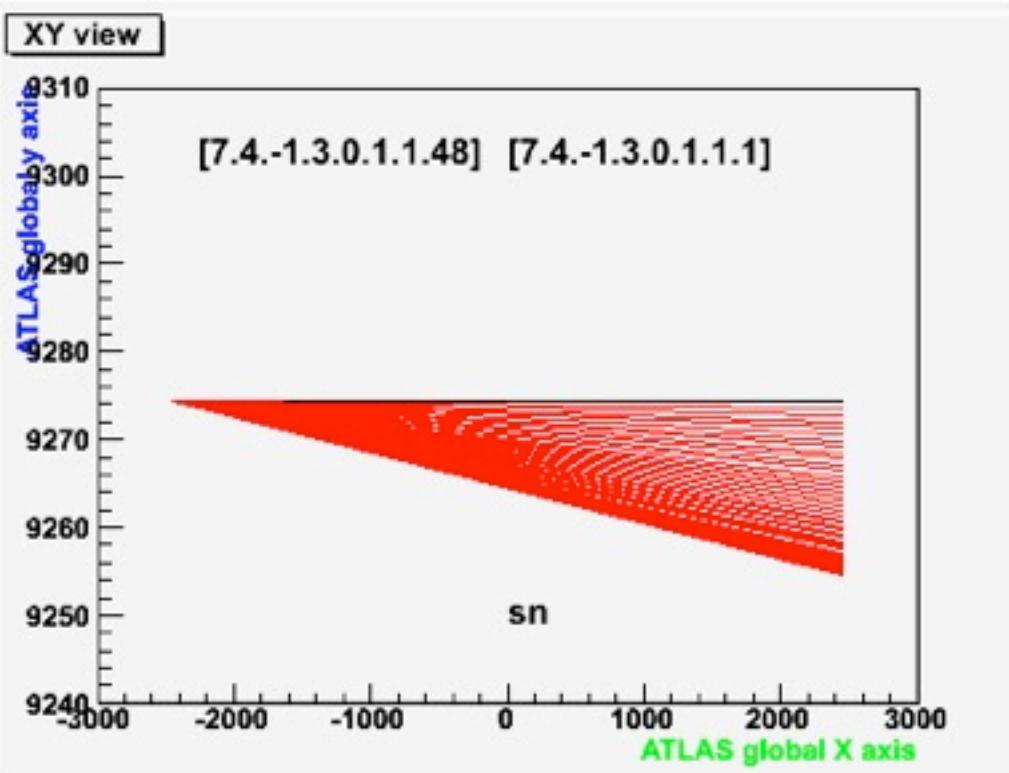


szl $\rightarrow -x, z, y$

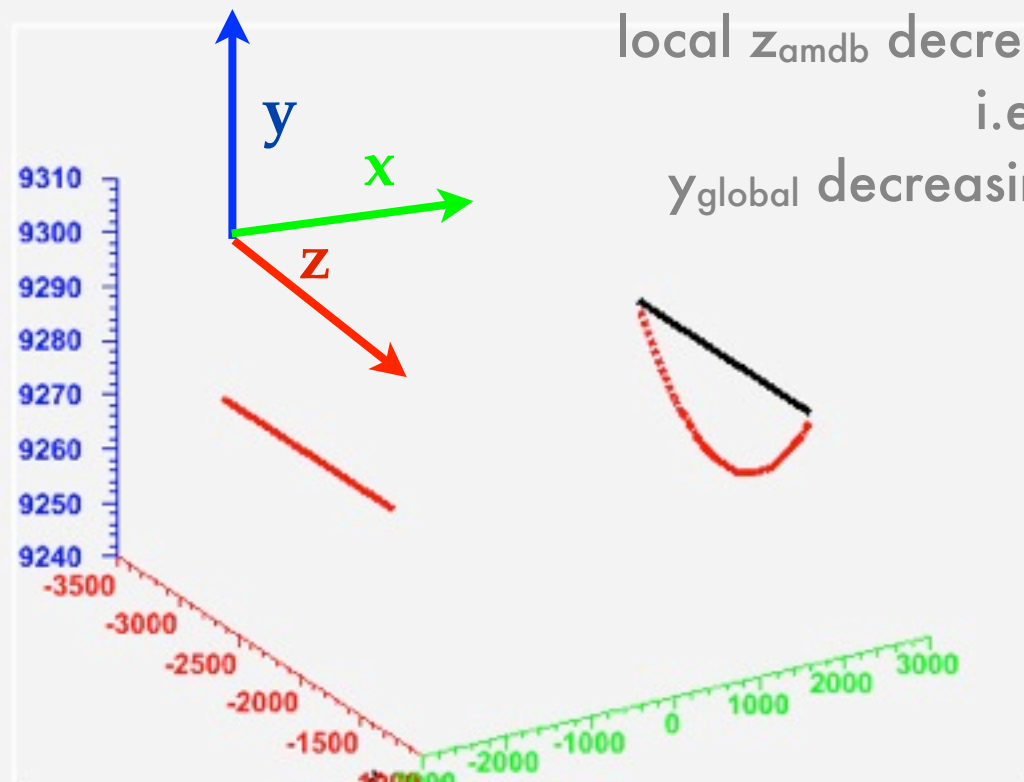
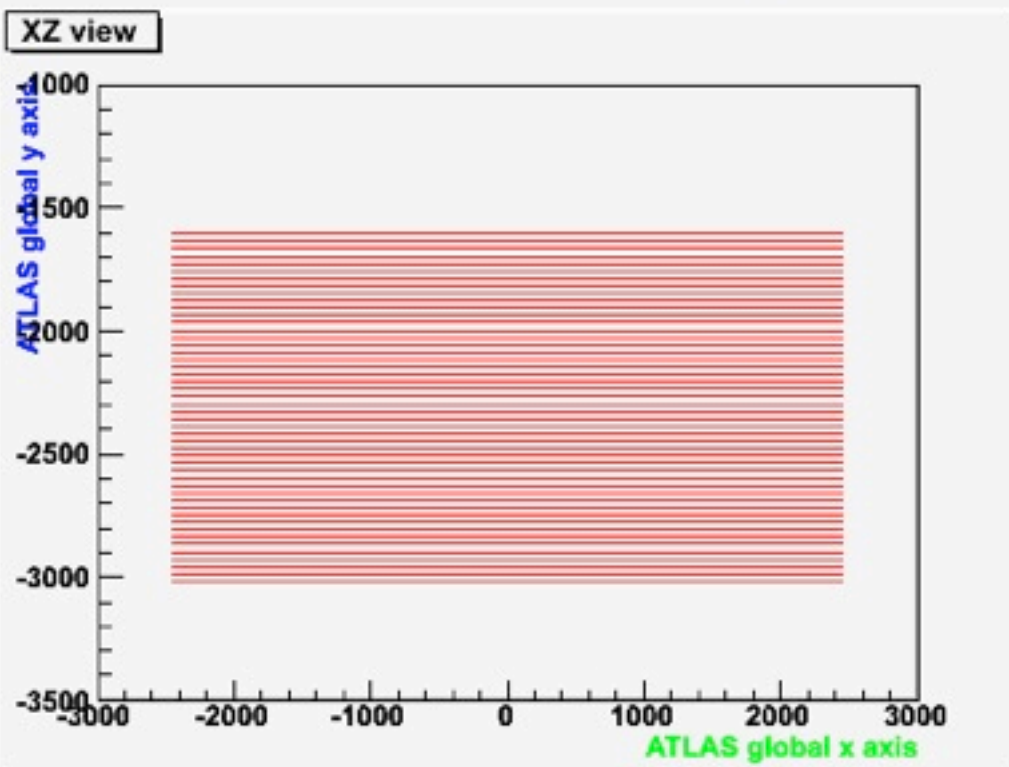


local z_{amdb} decreasing at $s_{amdb} < 0$
i.e.
 y_{global} decreasing at $x_{global} > 0$

sn=10mm BOLC

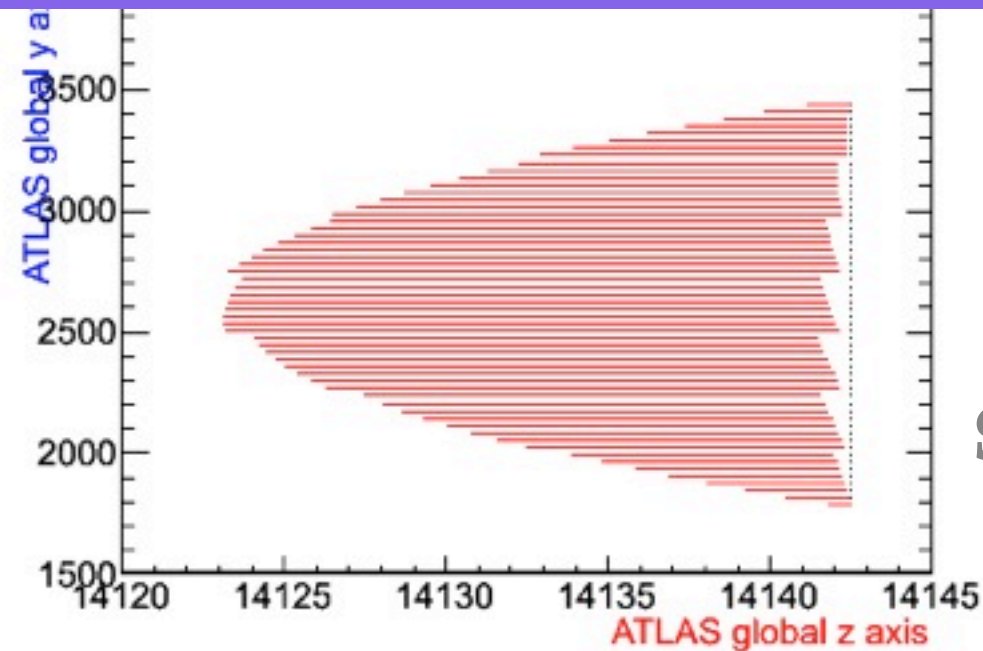
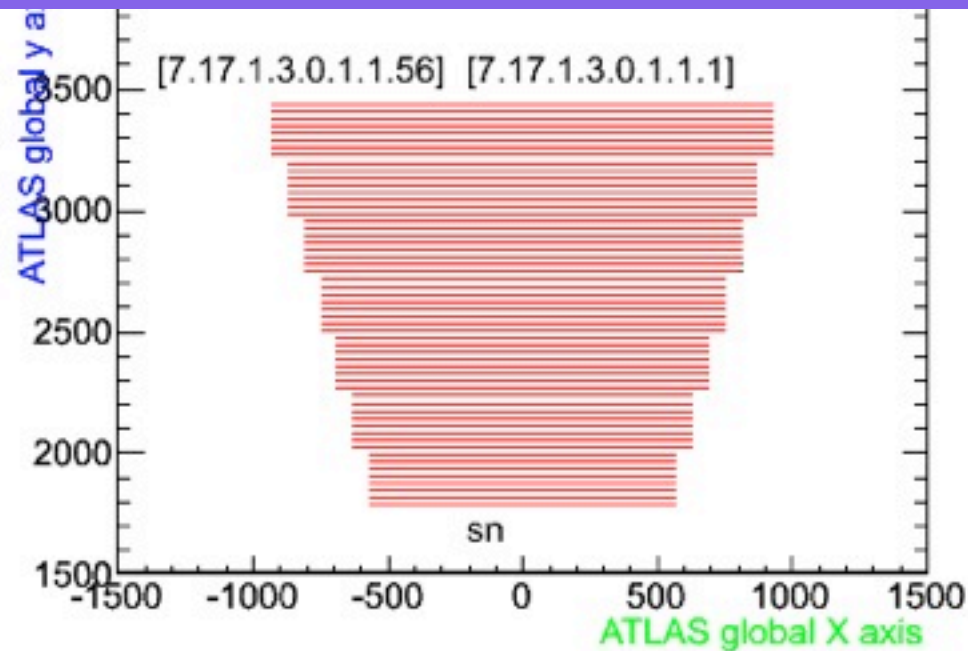


sz t \Rightarrow -x,z,y

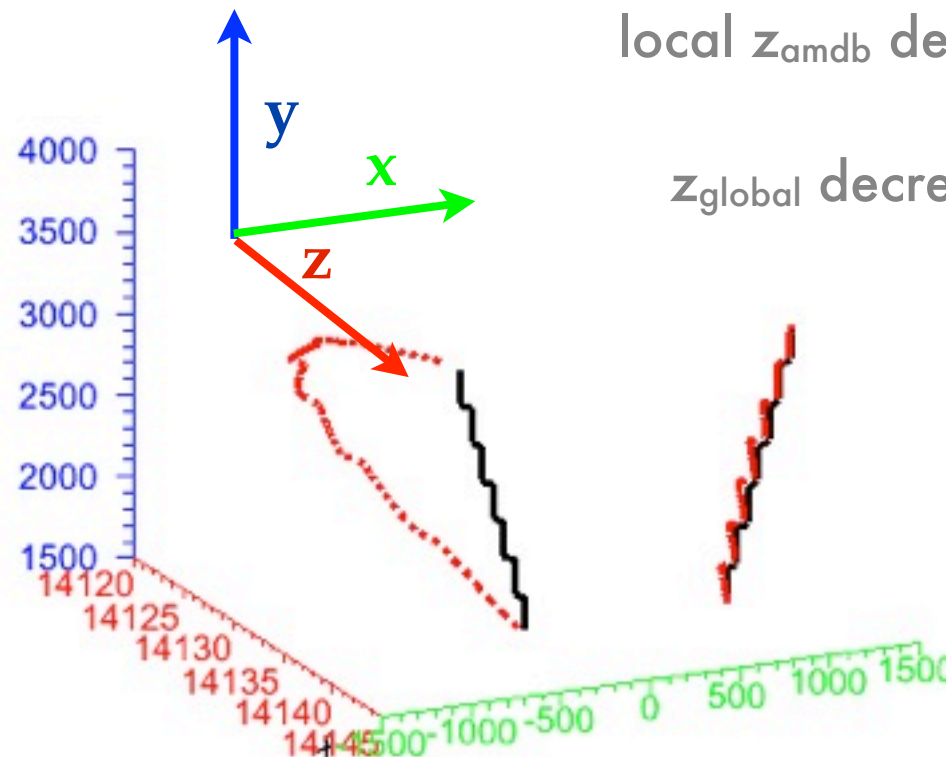
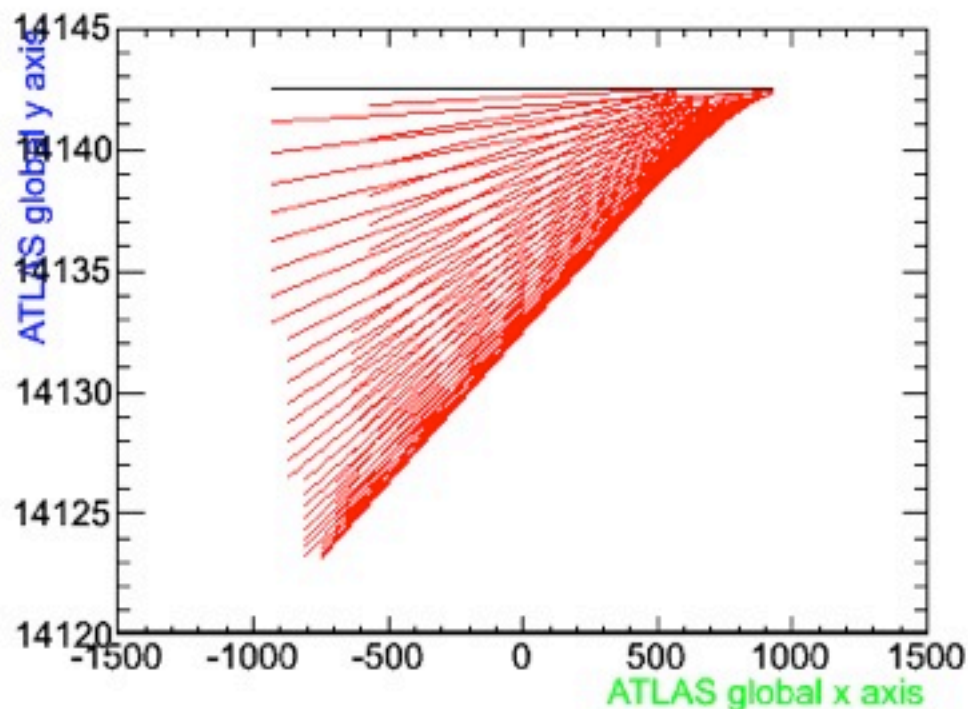


local z_{amdb} decreasing at $s_{amdb} < 0$
i.e.
 y_{global} decreasing at $x_{global} > 0$

sn=10mm EMLA

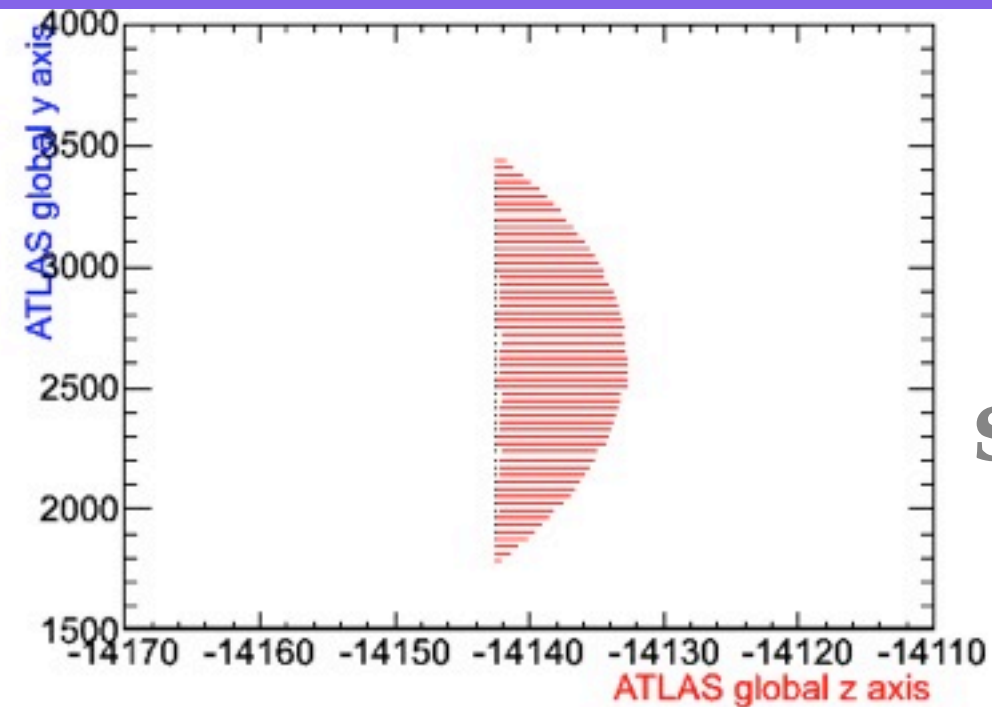
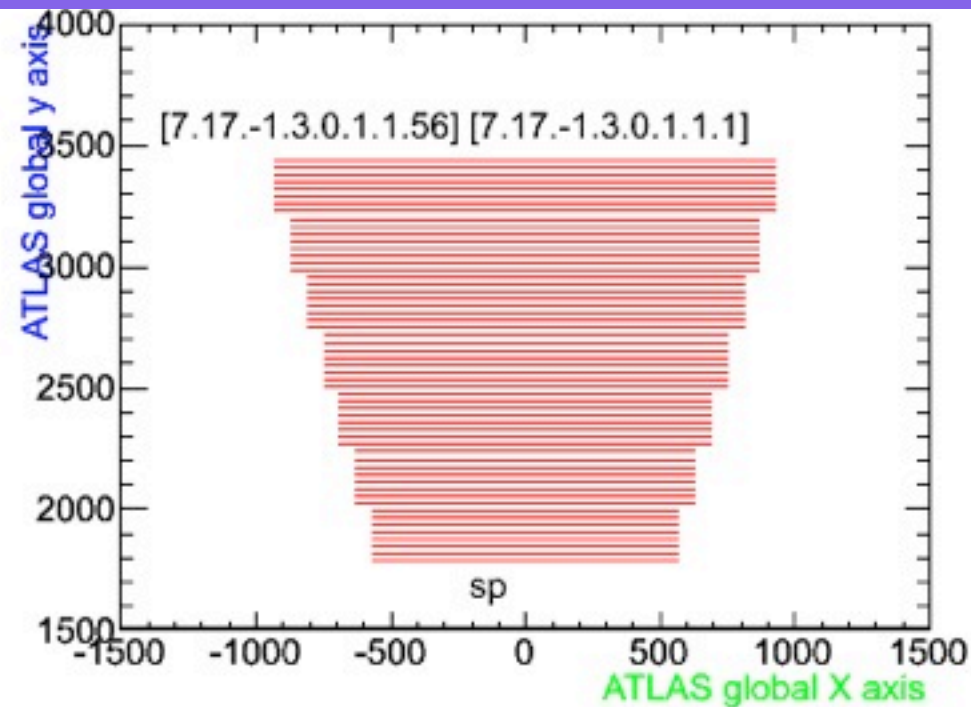


szl \rightarrow x,z,y

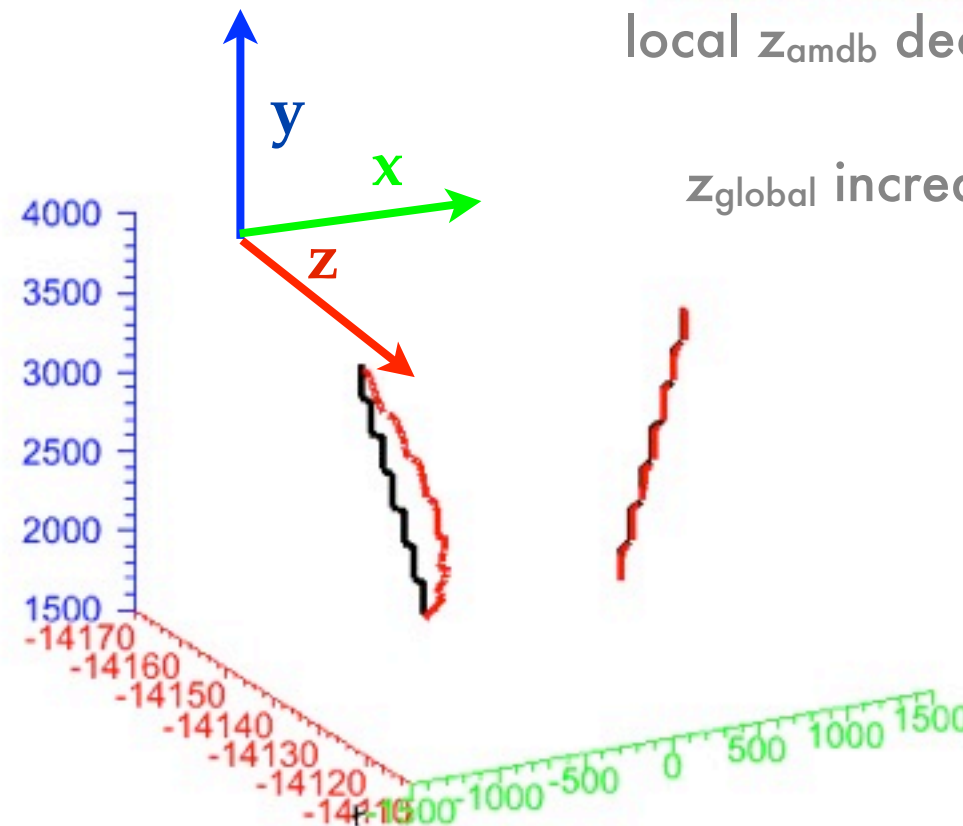
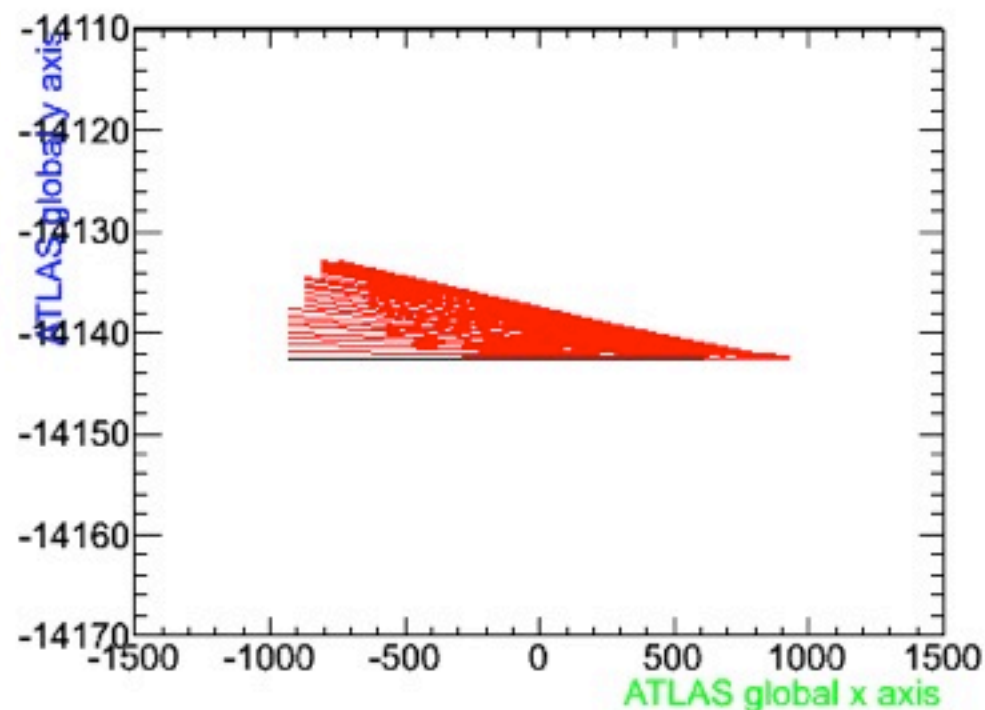


local z_{amdb} decreasing at $s_{amdb} < 0$
i.e.
 z_{global} decreasing at $x_{global} < 0$

sn=10mm EMLC



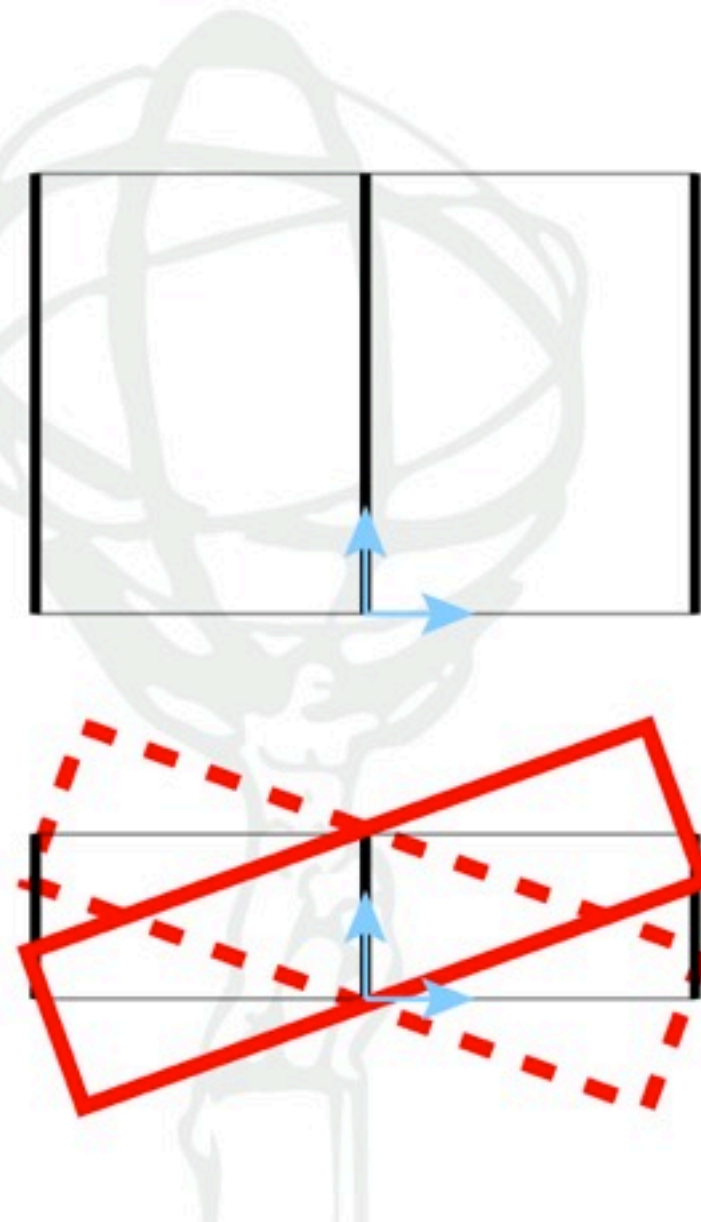
szr $\rightarrow -x, z, -y$



local z_{amdb} decreasing at $s_{amdb} < 0$
i.e.
 z_{global} increasing at $x_{global} < 0$

twist

Twist: tw (1 Parameter)



- **tw:**

out-of-plane rotation of both outer cross-plates in opposite directions, tubes remain straight

maximum out-of-plane shift (at corners) equals tw , positive for shift of corner at $s_{rel} = 1, z_{rel} = 1$ towards negative t

unit: mm

typical: $\mathcal{O}(100 \mu m)$

formula:

$$\phi = -tw \cdot s_{rel}$$

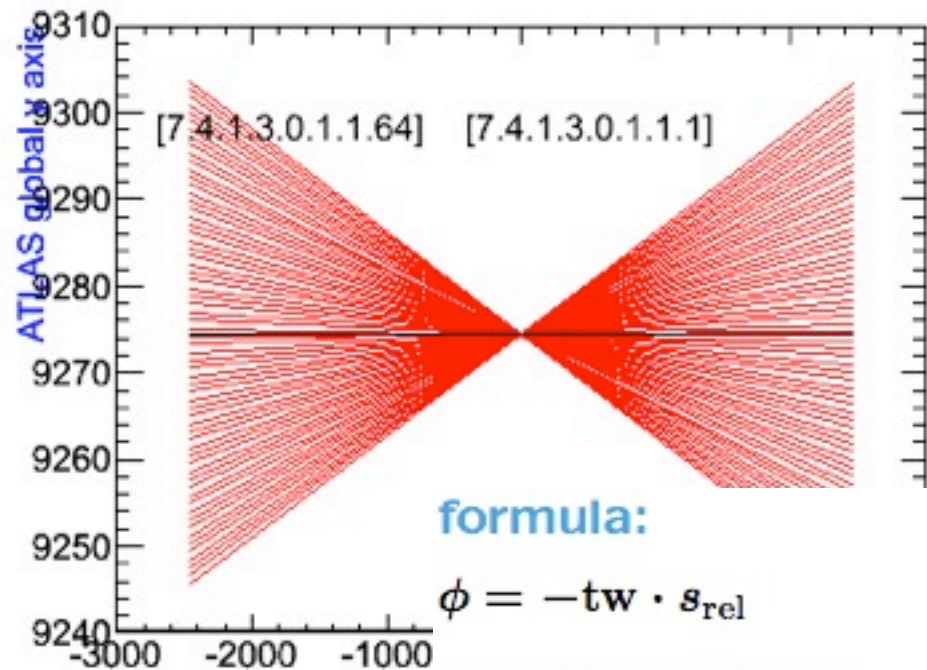
transformation:

$$s \rightarrow s$$

$$t \rightarrow t + \phi \cdot z_{rel}$$

$$z \rightarrow z - \phi \cdot t_{rel} \cdot \frac{\text{height}}{\text{length}}$$

tw=30mm BOLA



formula:

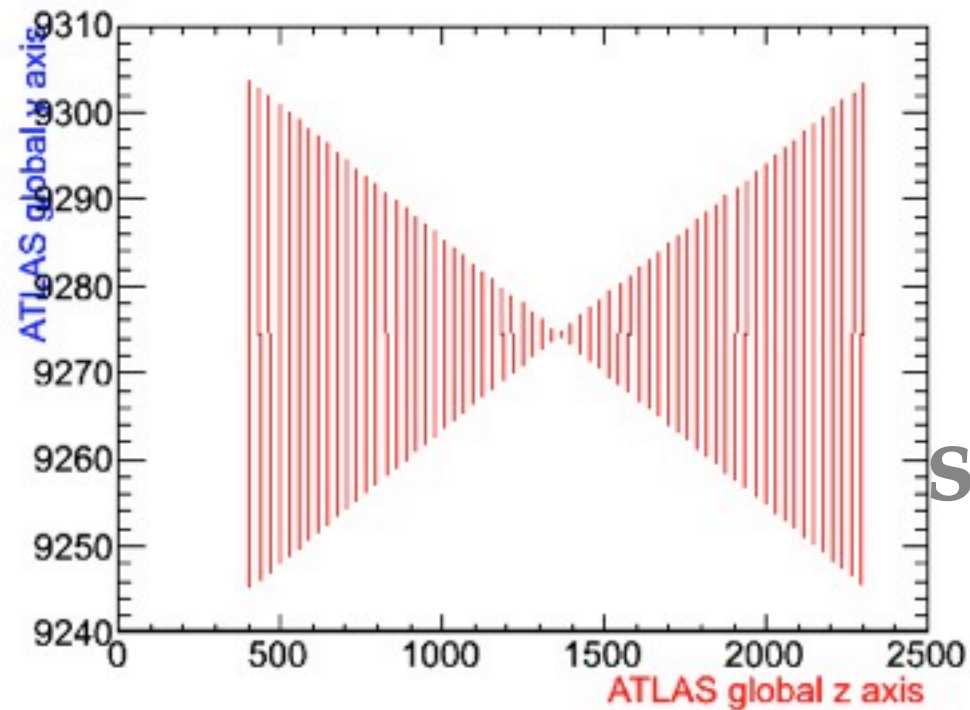
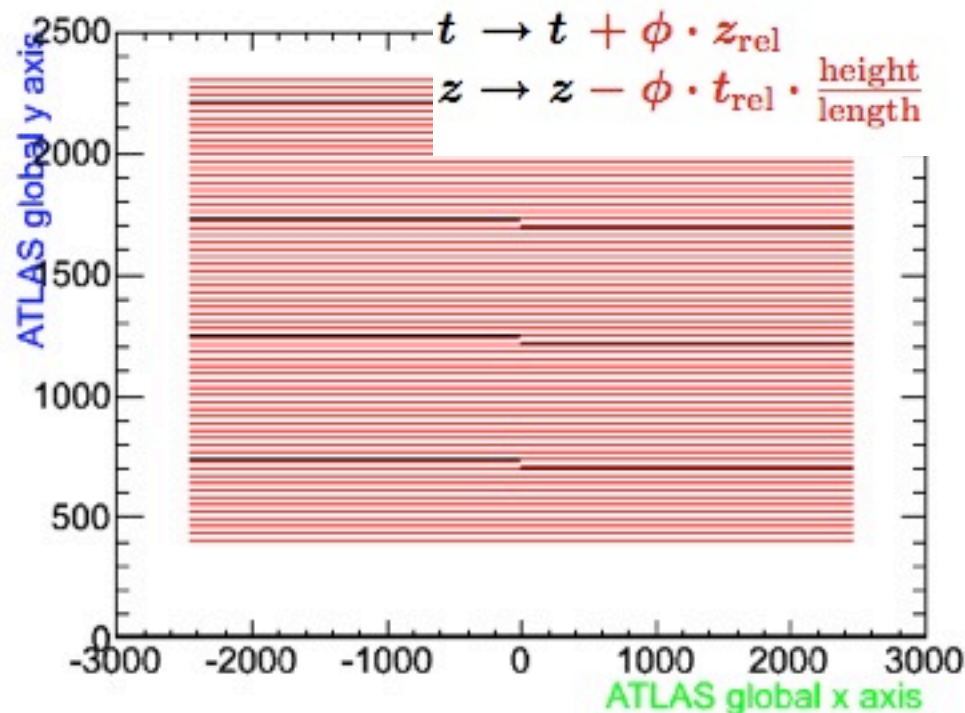
$$\phi = -tw \cdot s_{rel}$$

transformation:

$$s \rightarrow s$$

$$t \rightarrow t + \phi \cdot z_{rel}$$

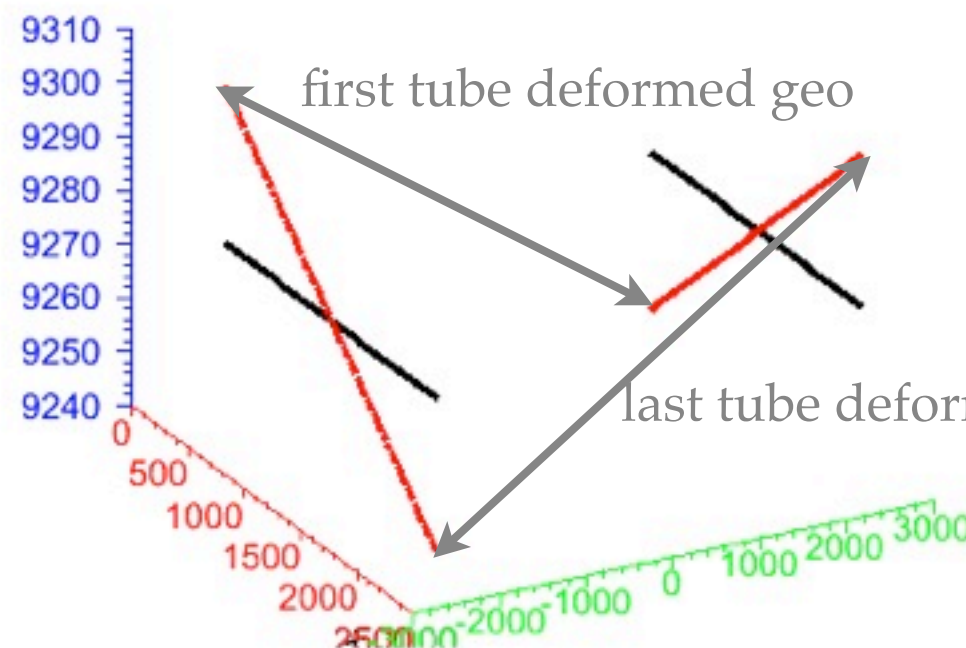
$$z \rightarrow z - \phi \cdot t_{rel} \cdot \frac{\text{height}}{\text{length}}$$



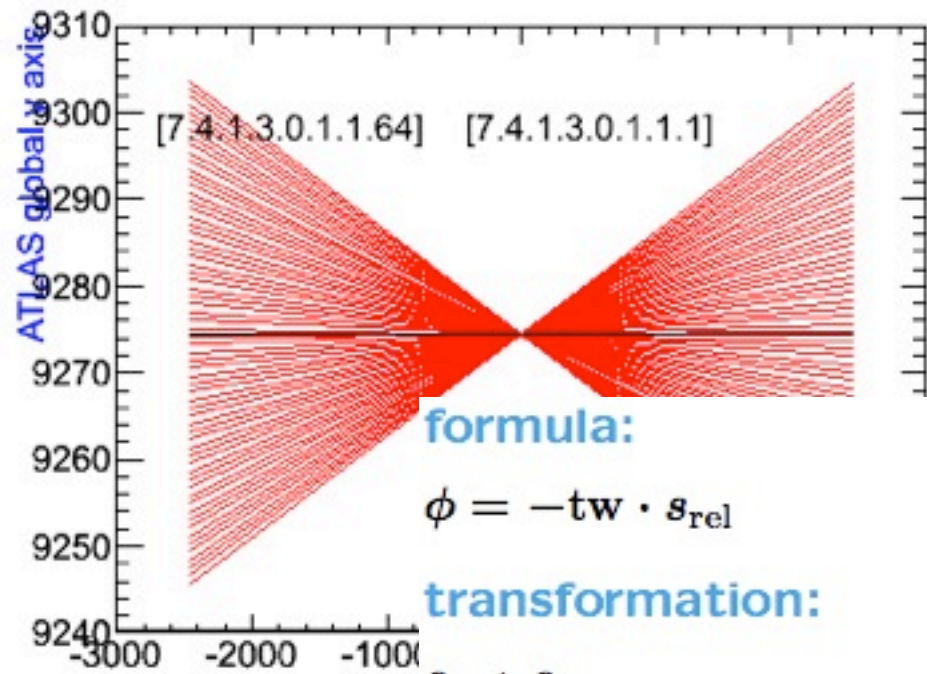
sz t \rightarrow -x,z,y

NOTE: in 2008 MGM and Aramys agreed on the tw effect - definition changed later to account for the z (amdb) correction

Here new MGM implementation of tw



tw=30mm BOLA

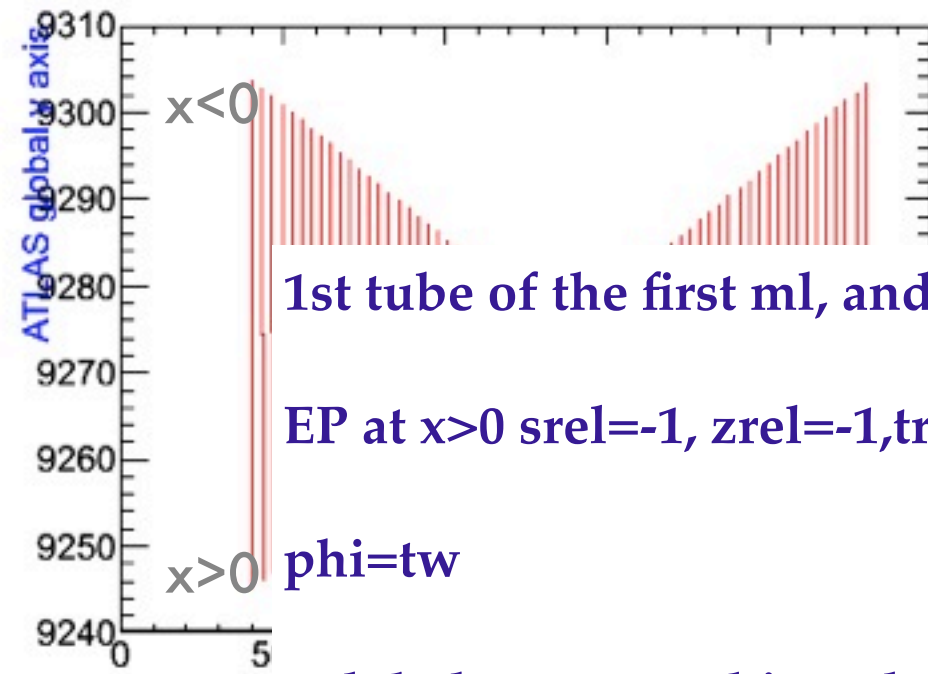


formula:

$$\phi = -tw \cdot s_{rel}$$

transformation:

$$\begin{aligned} s &\rightarrow s \\ t &\rightarrow t + \phi \cdot z_{rel} \\ z &\rightarrow z - \phi \cdot t_{rel} \cdot \frac{\text{height}}{\text{length}} \end{aligned}$$



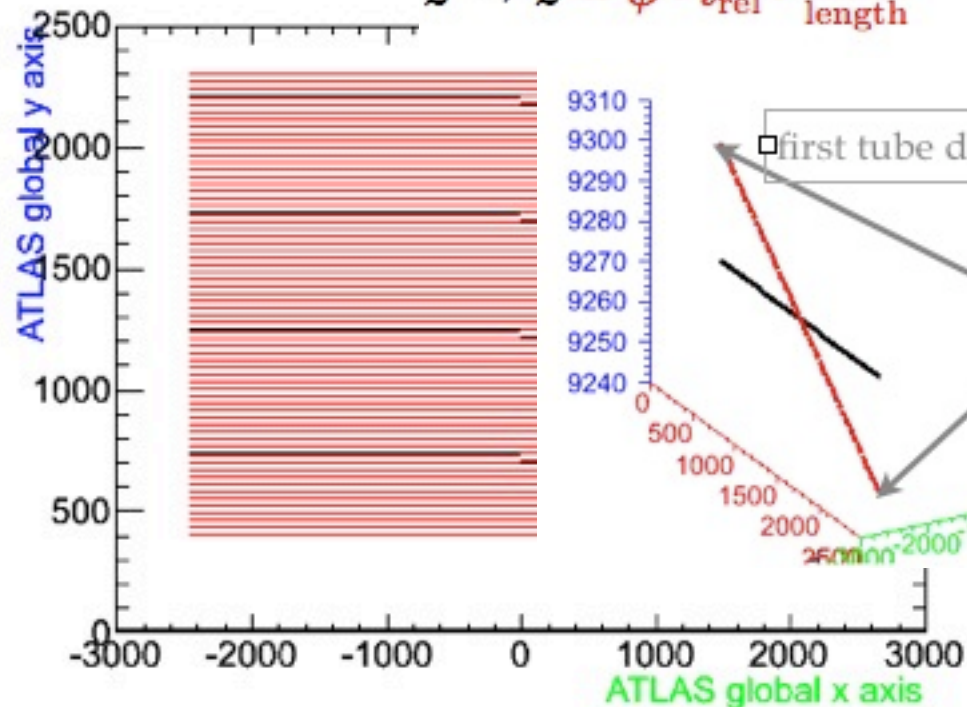
1st tube of the first ml, and tl

EP at x>0 srel=-1, zrel=-1, trel=-1

phi=tw

yglobal=t=tnom-phi <yglobalnom

zglobal=z=znom+phi*height/length>zglobaniminal



first tube deformed geo

last tube deformed geo

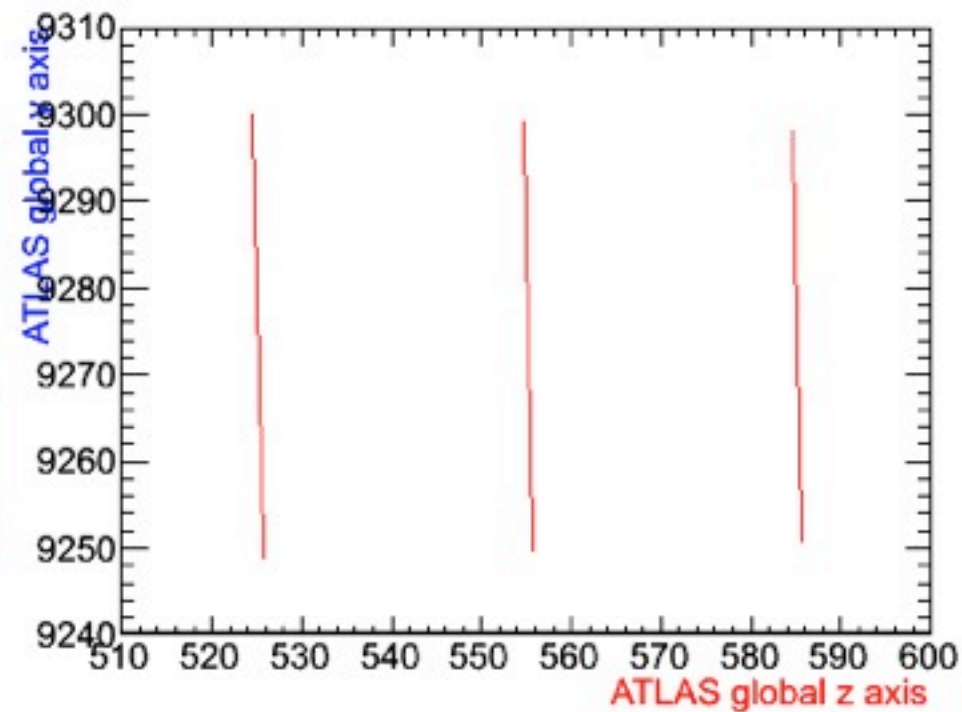
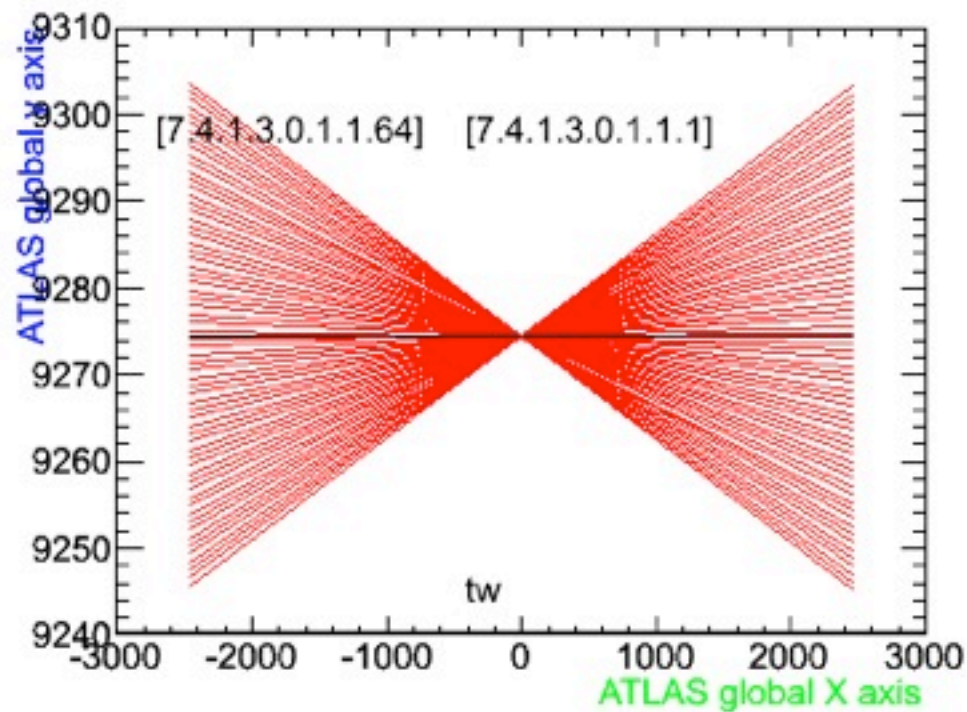
EP at x<0 srel=1, zrel=-1, trel=-1

phi=-tw

yglobal=t=tnom-phi >yglobalnom

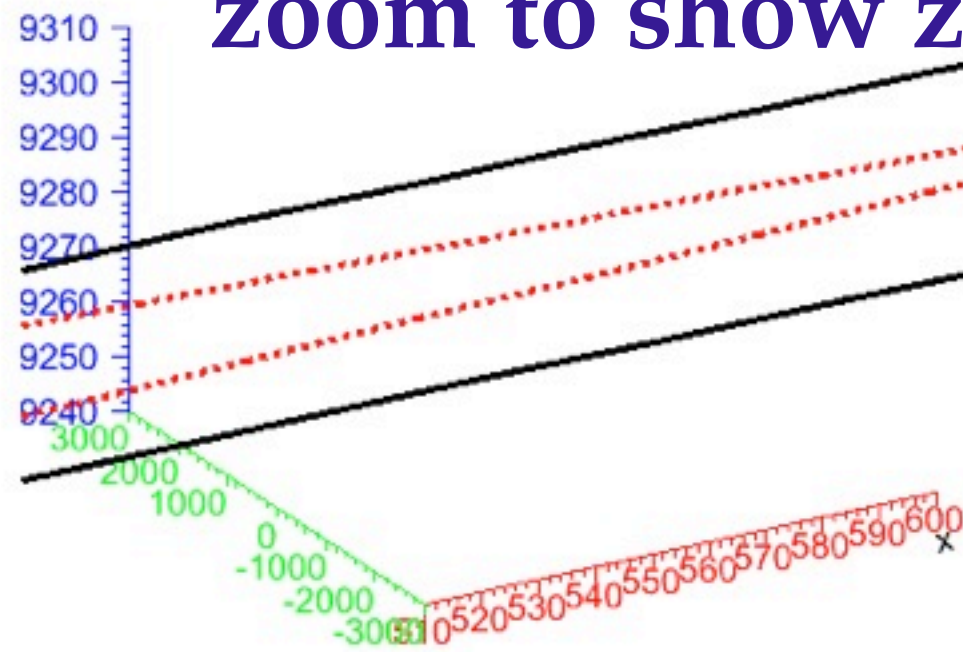
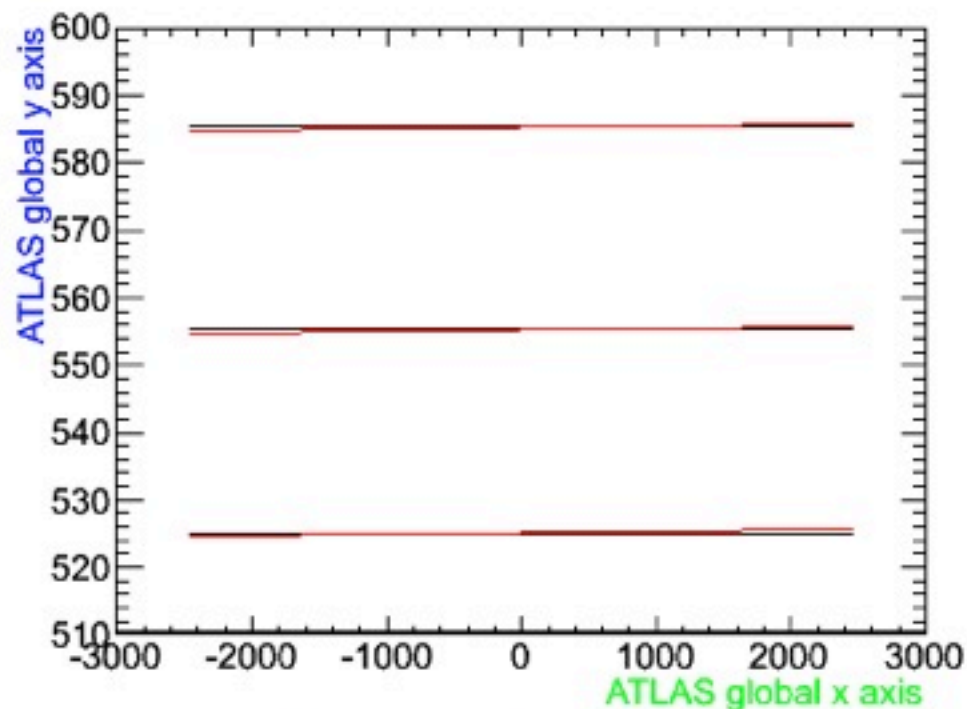
zglobal=z=znom+phi*hl<zglobaniminal

tw=30mm BOLA

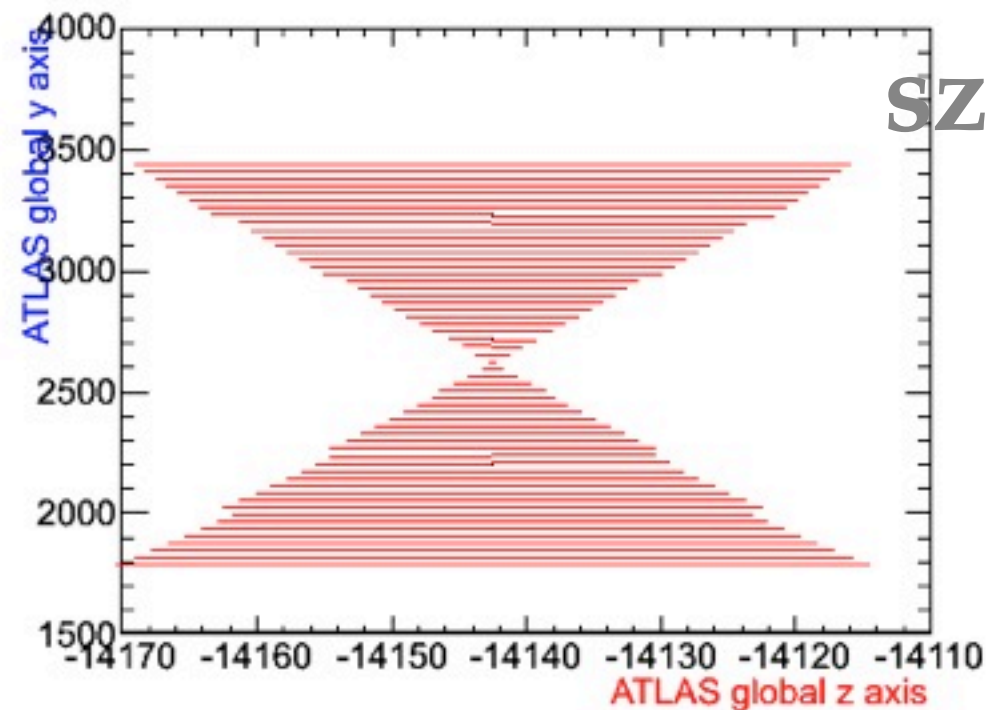
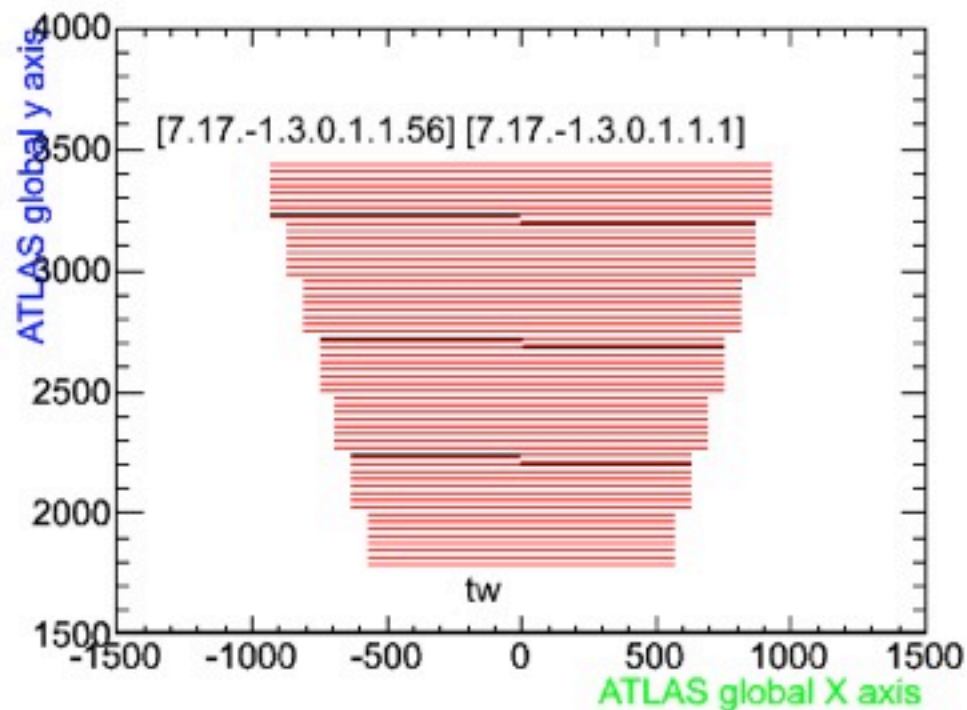


Here new MGM implementation of tw

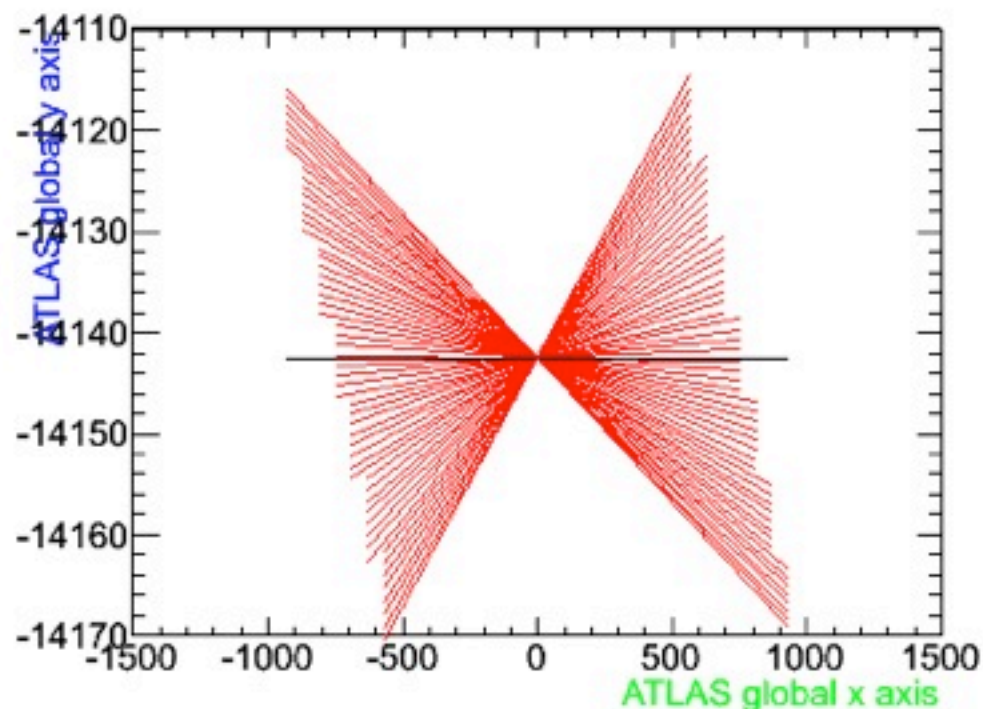
zoom to show z effect



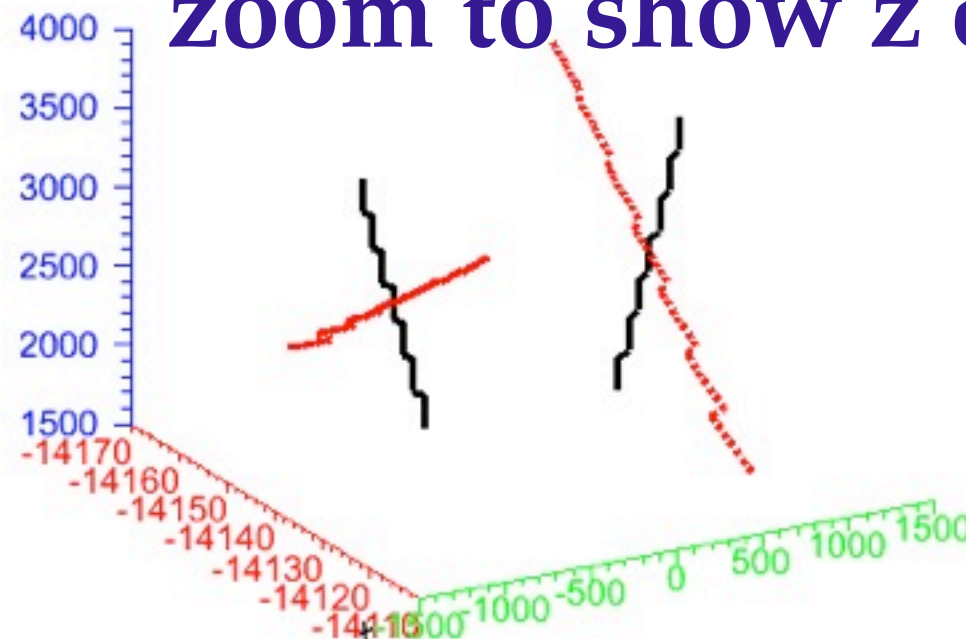
tw=30mm EML-C



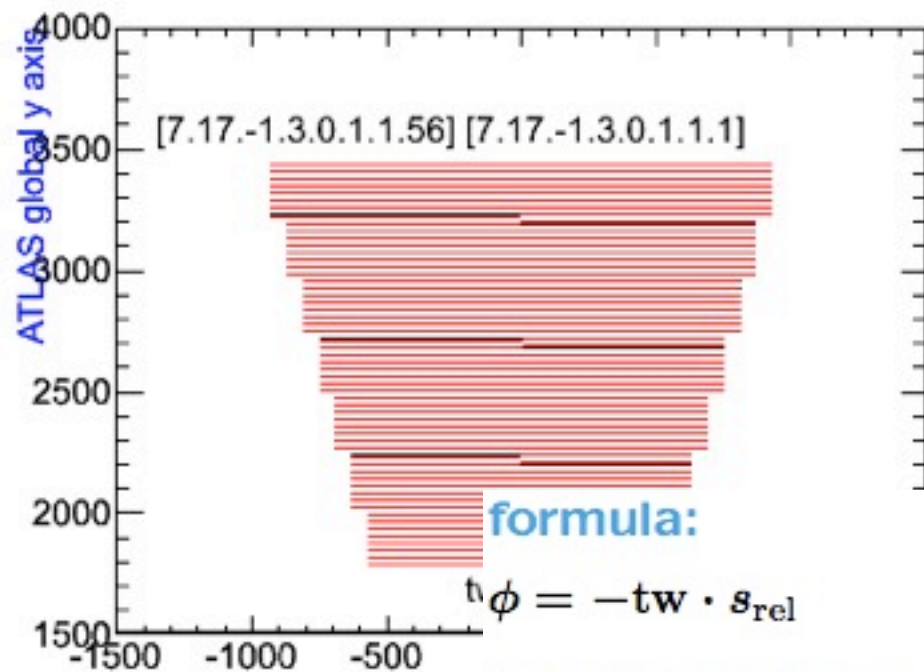
Here new MGM implementation of tw



zoom to show z effect



tw=30mm EML-C



formula:

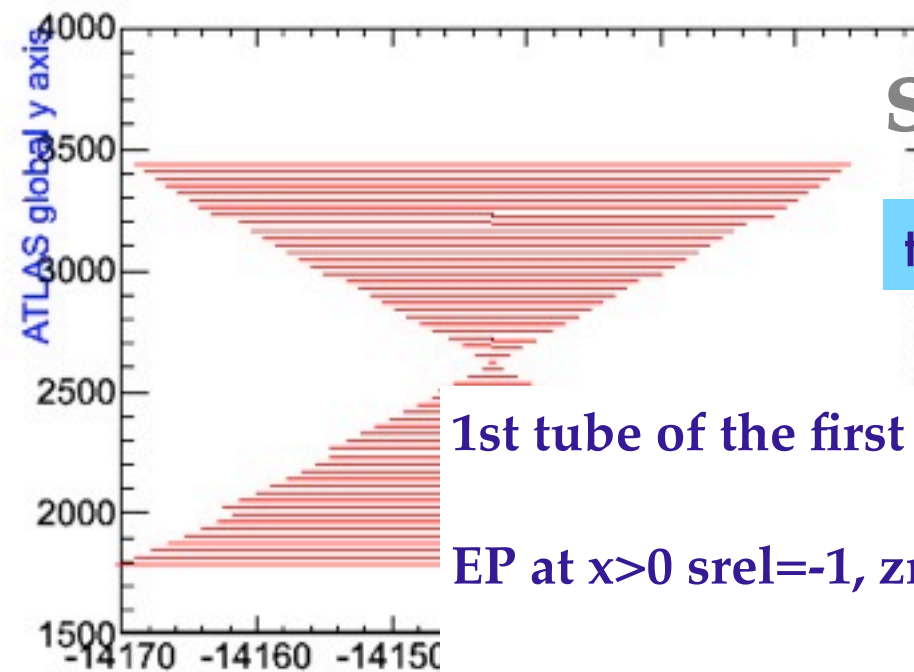
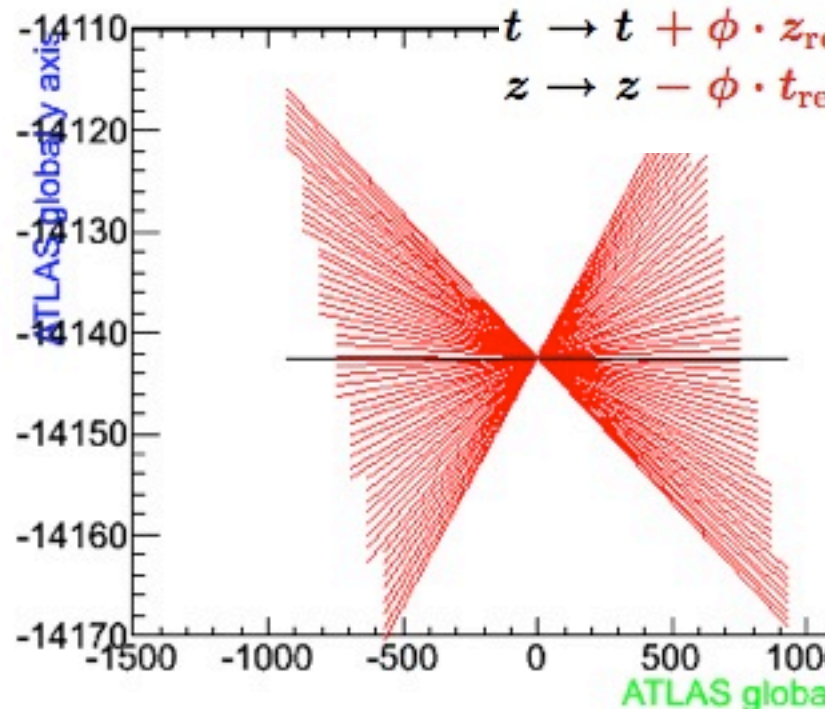
$$\phi = -tw \cdot s_{rel}$$

transformation:

$$s \rightarrow s$$

$$t \rightarrow t + \phi \cdot z_{rel}$$

$$z \rightarrow z - \phi \cdot t_{rel} \cdot \frac{\text{height}}{\text{length}}$$



sz t \rightarrow -x, y, -z

tw conventions OK

1st tube of the first ml, and tl

EP at $x > 0$ $s_{rel} = -1$, $z_{rel} = -1$, $t_{rel} = -1$

$\phi = tw$

$y_{global} = z = z_{nom} + \phi \cdot h/l > y_{globalnom}$

$z_{global} = -t = -t_{nom} + \phi > z_{globalnominal}$

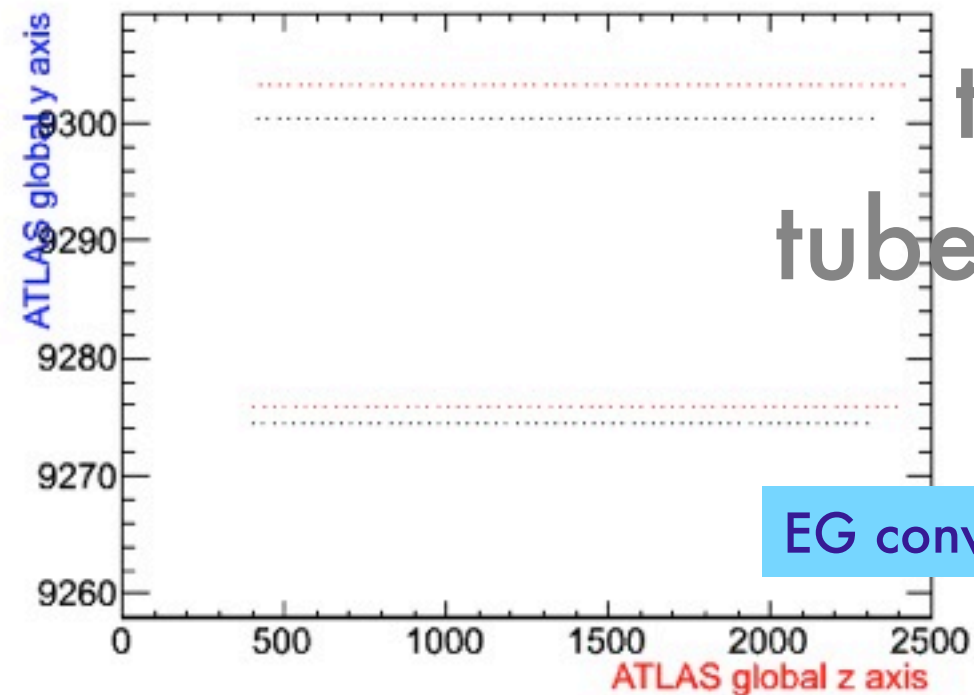
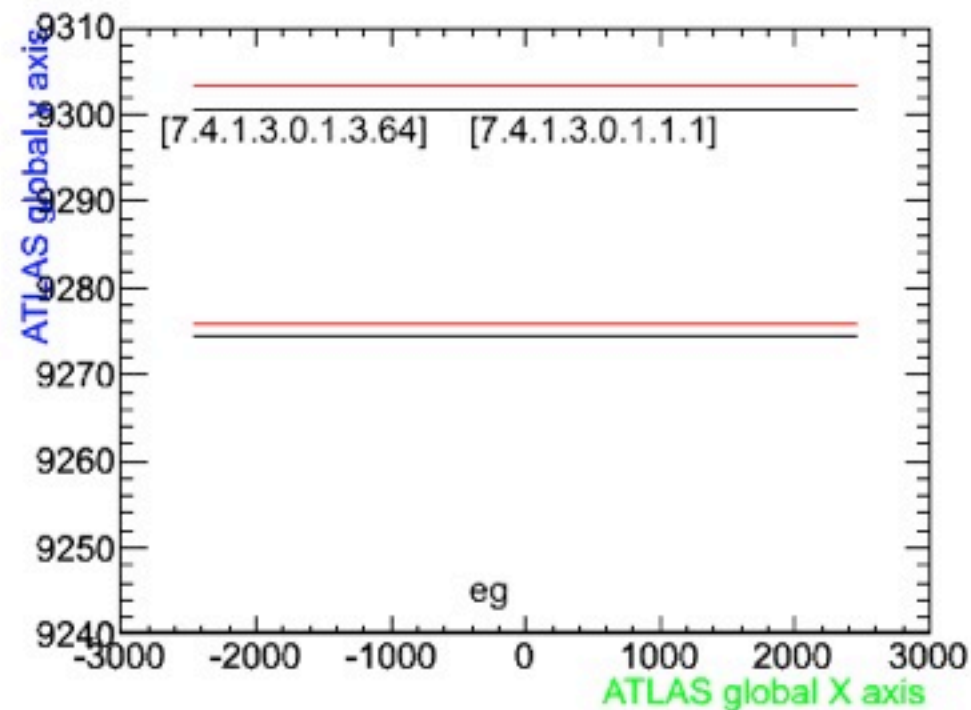
EP at $x < 0$ $s_{rel} = 1$, $z_{rel} = -1$, $t_{rel} = -1$

$\phi = -tw$

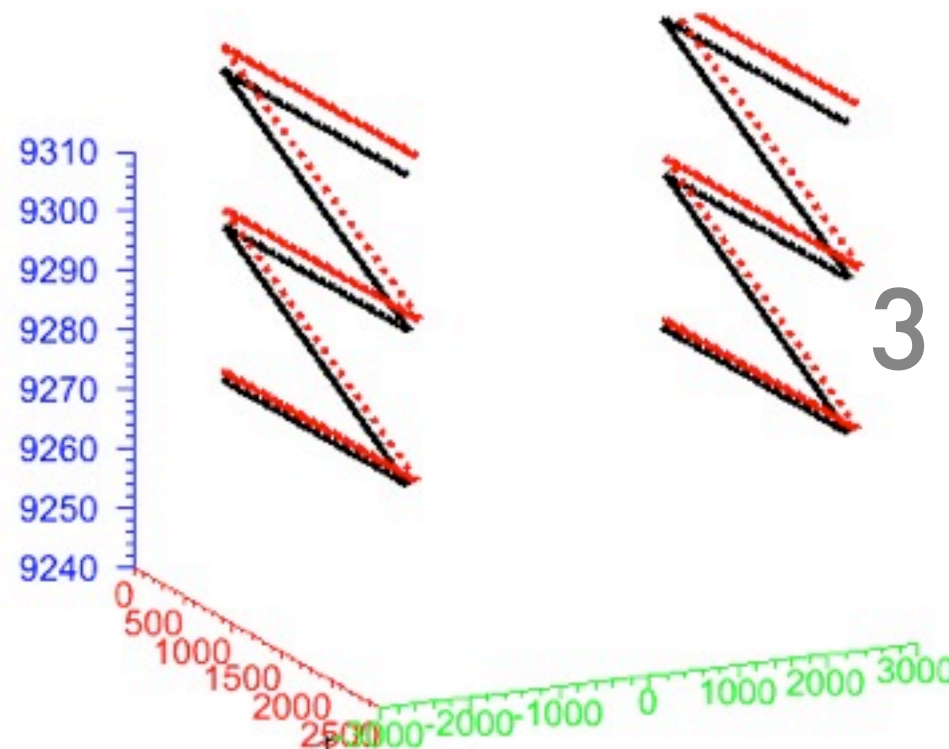
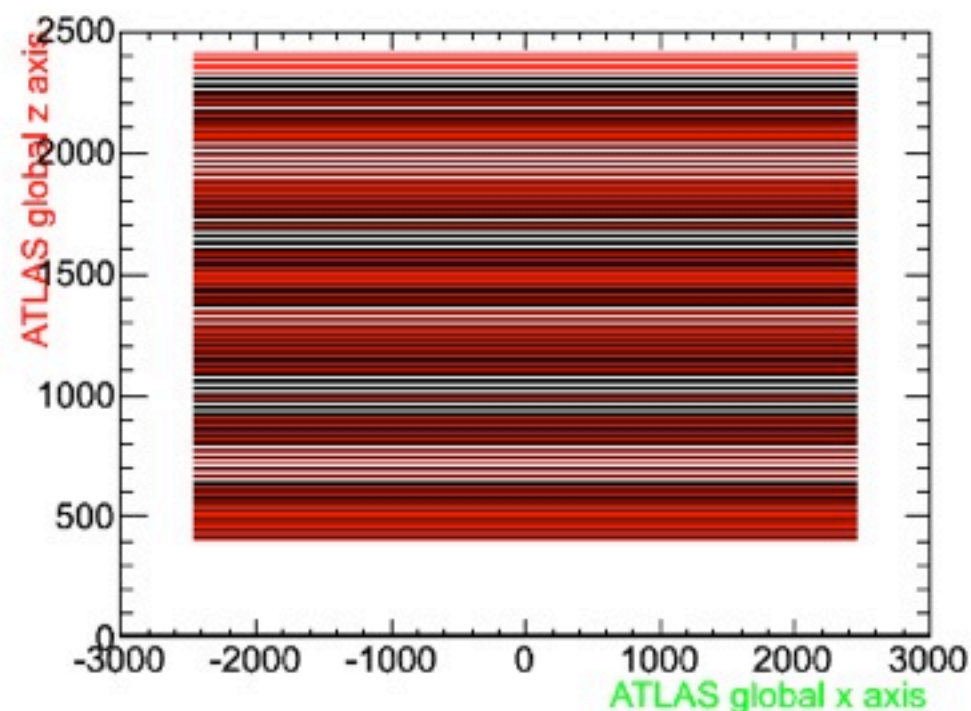
$y_{global} = z = z_{nom} + \phi \cdot h/l < y_{globalnom}$

$z_{global} = -t = -t_{nom} + \phi < z_{globalnominal}$

eg=0.05 BOL-A

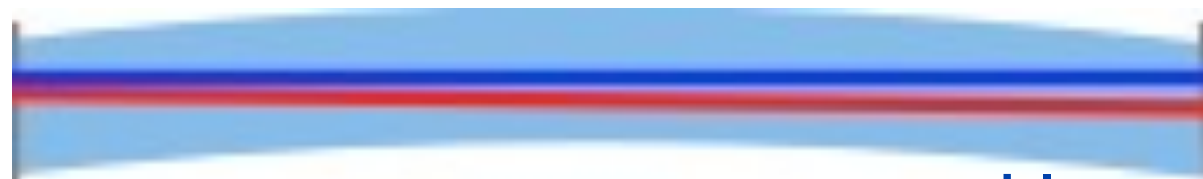


EG conventions OK



3 tube layers

ep, en



deformed tube

blue = nominal wire position
for undeformed tube

red = wire (straight) in the
deformed tube

ep, en imply a change in the
wire trajectory+the wire is not
at the center of the tube at all s

stations with B-line fixed point not at 0,0,0 in amdb szt frame

MuGM:MuonStation
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MuGM:MuonStation
MuGM:MuonStation

DEBUG Station BIR at zi/fi 1/6 setting fixed point for B-lines at s0,z0,t0 = 0 180.21 0
DEBUG Station BIR at zi/fi -2/6 setting fixed point for B-lines at s0,z0,t0 = 0 90.105 0
DEBUG Station BIR at zi/fi -5/6 setting fixed point for B-lines at s0,z0,t0 = 0 90.105 0
DEBUG Station BIR at zi/fi -2/8 setting fixed point for B-lines at s0,z0,t0 = 0 90.105 0
DEBUG Station BIR at zi/fi -5/8 setting fixed point for B-lines at s0,z0,t0 = 0 90.105 0
DEBUG Station BIR at zi/fi 4/8 setting fixed point for B-lines at s0,z0,t0 = 0 90.105 0
DEBUG Station BIR at zi/fi 1/8 setting fixed point for B-lines at s0,z0,t0 = 0 180.21 0
DEBUG Station BIR at zi/fi 4/6 setting fixed point for B-lines at s0,z0,t0 = 0 90.105 0
DEBUG Station BMF at zi/fi 3/6 setting fixed point for B-lines at s0,z0,t0 = 0 0 144
DEBUG Station BMF at zi/fi 3/7 setting fixed point for B-lines at s0,z0,t0 = 0 0 144
DEBUG Station BMF at zi/fi 2/6 setting fixed point for B-lines at s0,z0,t0 = 0 0 144
DEBUG Station BMF at zi/fi 2/7 setting fixed point for B-lines at s0,z0,t0 = 0 0 144
DEBUG Station BMF at zi/fi 1/6 setting fixed point for B-lines at s0,z0,t0 = 0 0 144
DEBUG Station BMF at zi/fi 1/7 setting fixed point for B-lines at s0,z0,t0 = 0 0 144
DEBUG Station BMF at zi/fi -1/6 setting fixed point for B-lines at s0,z0,t0 = 0 -2 144
DEBUG Station BMF at zi/fi -1/7 setting fixed point for B-lines at s0,z0,t0 = 0 -2 144
DEBUG Station BMF at zi/fi -2/6 setting fixed point for B-lines at s0,z0,t0 = 0 -2 144
DEBUG Station BMF at zi/fi -2/7 setting fixed point for B-lines at s0,z0,t0 = 0 -2 144
DEBUG Station BMF at zi/fi -3/6 setting fixed point for B-lines at s0,z0,t0 = 0 -1.681 144
DEBUG Station BMF at zi/fi -3/7 setting fixed point for B-lines at s0,z0,t0 = 0 -1.681 144

stations with B-line fixed point not at
0,0,0 in amdb szt frame

[illegible]

DEBUG Station BML at zi/fi -2/4 setting fixed point for B-lines at s0,z0,t0 =	0	-1.961	139.5
DEBUG Station BML at zi/fi -2/5 setting fixed point for B-lines at s0,z0,t0 =	0	-1.961	139.5
DEBUG Station BML at zi/fi -2/6 setting fixed point for B-lines at s0,z0,t0 =	0	-1.961	139.5
DEBUG Station BML at zi/fi -2/7 setting fixed point for B-lines at s0,z0,t0 =	0	-1.961	139.5
DEBUG Station BML at zi/fi -2/8 setting fixed point for B-lines at s0,z0,t0 =	0	-1.961	139.5
DEBUG Station BML at zi/fi -5/1 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -5/2 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -5/3 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -5/4 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -5/5 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -5/6 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -5/8 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -4/1 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -4/2 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -4/3 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -4/4 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -4/5 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -4/6 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -4/7 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -4/8 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -1/6 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -1/8 setting fixed point for B-lines at s0,z0,t0 =	0	-1.401	139.5
DEBUG Station BML at zi/fi -6/1 setting fixed point for B-lines at s0,z0,t0 =	0	-1.681	139.5
DEBUG Station BML at zi/fi -6/2 setting fixed point for B-lines at s0,z0,t0 =	0	-1.681	139.5
DEBUG Station BML at zi/fi -6/3 setting fixed point for B-lines at s0,z0,t0 =	0	-1.681	139.5
DEBUG Station BML at zi/fi -6/4 setting fixed point for B-lines at s0,z0,t0 =	0	-1.681	139.5
DEBUG Station BML at zi/fi -6/5 setting fixed point for B-lines at s0,z0,t0 =	0	-1.681	139.5
DEBUG Station BML at zi/fi -6/6 setting fixed point for B-lines at s0,z0,t0 =	0	-1.681	139.5
DEBUG Station BML at zi/fi -6/8 setting fixed point for B-lines at s0,z0,t0 =	0	-1.681	139.5

InFN Lecce and Dip. Fisica, Univ. del SalentoCERN Muon SW Feb 1st, 2018